



Institut **Langevin**  
ONDES ET IMAGES

# Correlations of electromagnetic noise

Julien de Rosny – Matthieu Davy – Luis Ruigger – Mathias Fink



# A short introduction

# Electromagnetism

Electromagnetic force?

\* Interactions between moving charged particles (electrons, protons, ...)

\* When charges are oscillating : interaction is a wave because of the coupling between magnetic and electric fields



Maxwell equations

**E** : Electric field

**H** : magnetic field

$$\nabla \cdot \mathbf{E} = \frac{\rho}{\epsilon}$$

$\epsilon$  : Permittivity

$$\nabla \cdot \mathbf{H} = 0$$

$M$  : Permeability

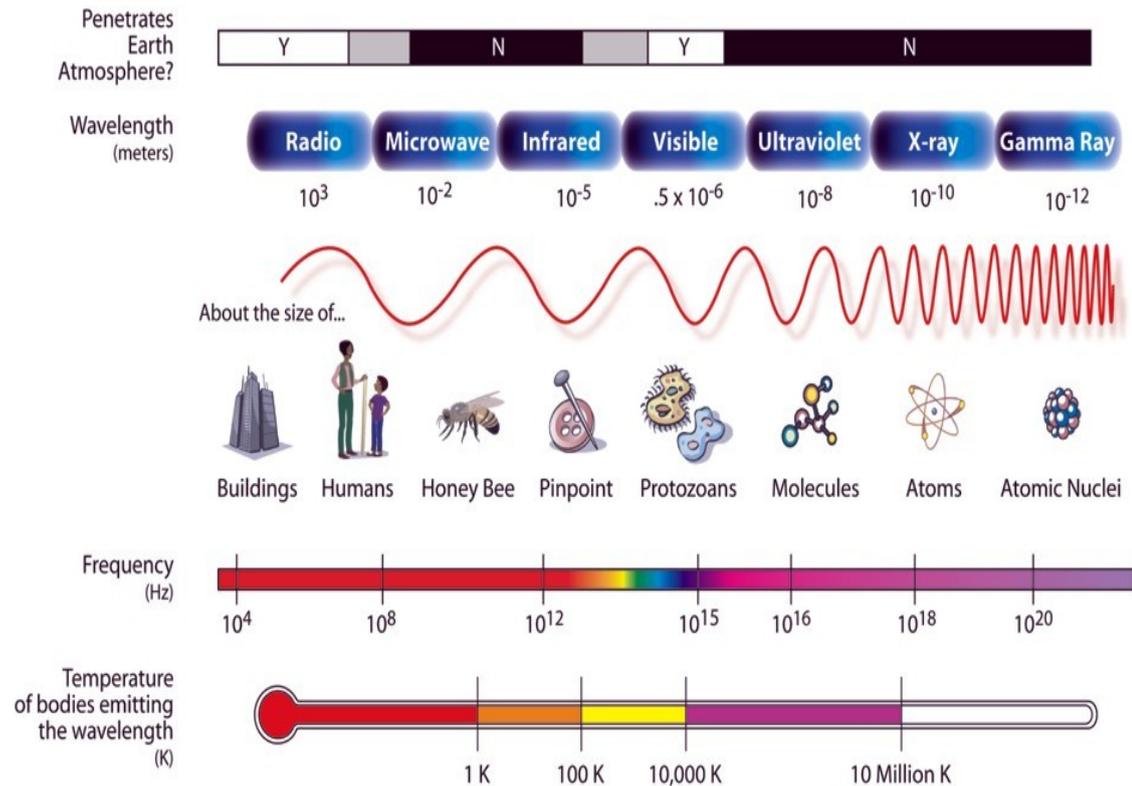
$$\nabla \times \mathbf{E} = -\mu \partial_t \mathbf{H}$$

$$\nabla \times \mathbf{H} = \mathbf{J} + \epsilon \partial_t \mathbf{E}$$

Coupling  $\rightarrow$  wave  
 $c = 1/\sqrt{(\mu\epsilon)}$

Polarizations : Vertical – Horizontal – circular Left and Right  
 No longitudinal wave

## THE ELECTROMAGNETIC SPECTRUM



Source : NASA

# Main sources of noise

- Artificial ones :
  - Long range TV and Radio broadcast
  - Short range Cell Phone (GSM-2G-3G-4G) – WIFI
- Natural ones :
  - Cosmic noise (30MHz-> 300GHz)
  - Atmospheric noise (30kHz->30MHz) Ionosphere
  - Thermal radiation of solids

# Overview of the talk

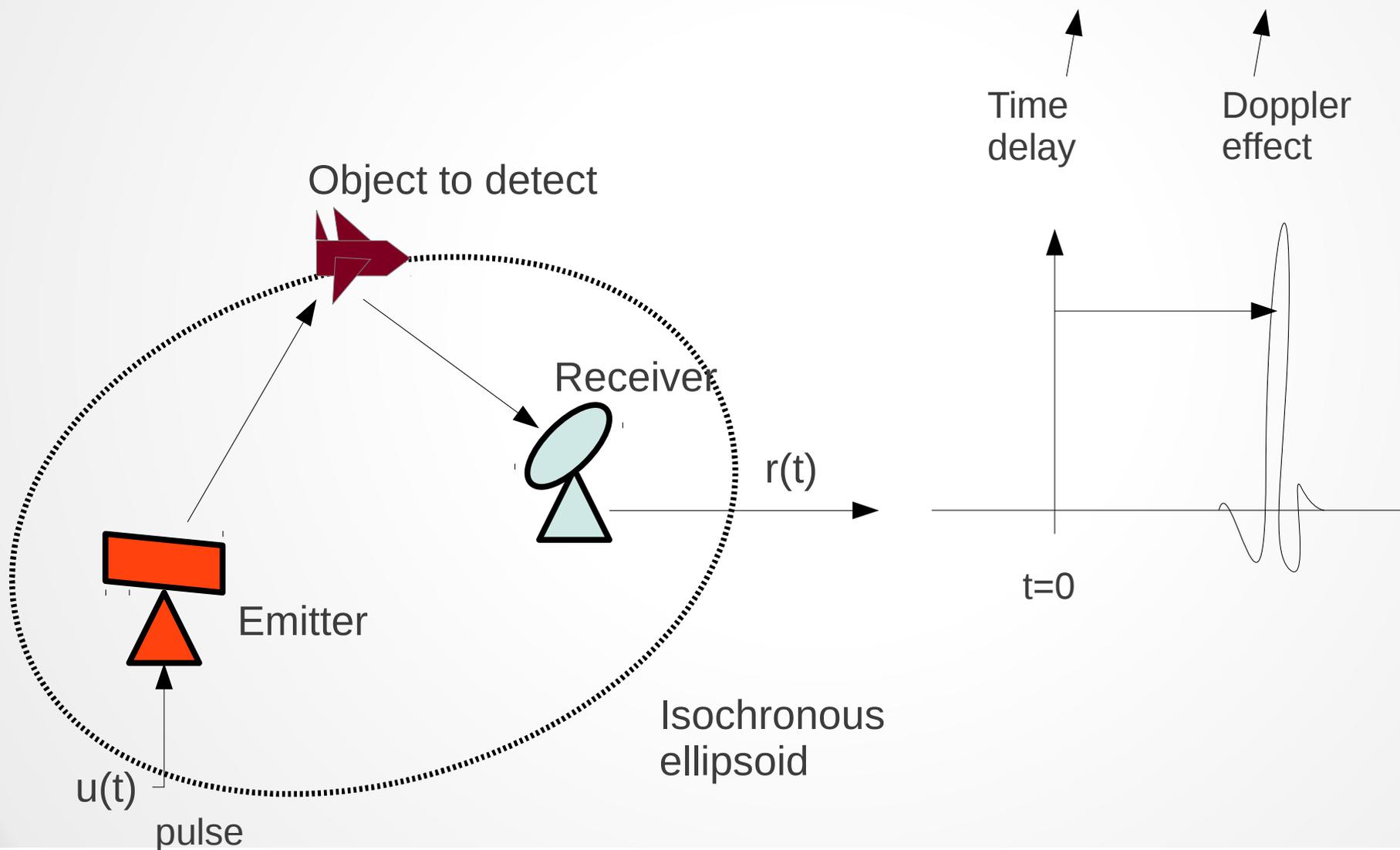
- 1) Bistatic RADAR using illuminators of opportunity
- 2) WiFi Imaging
- 3) Cross-correlations in reverberating media
- 4) Cross-correlations of thermal noise in cavities

# Bistatic noise detection

# Active Bistatic Radar

Controlled source (pulses – sweep - ...)

$$\varphi(\tau, \delta f) = \int u(t) r(t - \tau) \exp(-i 2\pi \delta f t) dt$$



# Active Bistatic Radar

Noise sources (TNT, FM, GSM, ...)

Correlation with doppler effect

$$\varphi(\tau, \delta f) = \int u(t) r(t - \tau) \exp(-i 2 \pi \delta f t) dt$$

Time delay

Doppler effect

Object to detected



$r(t)$  Receiver

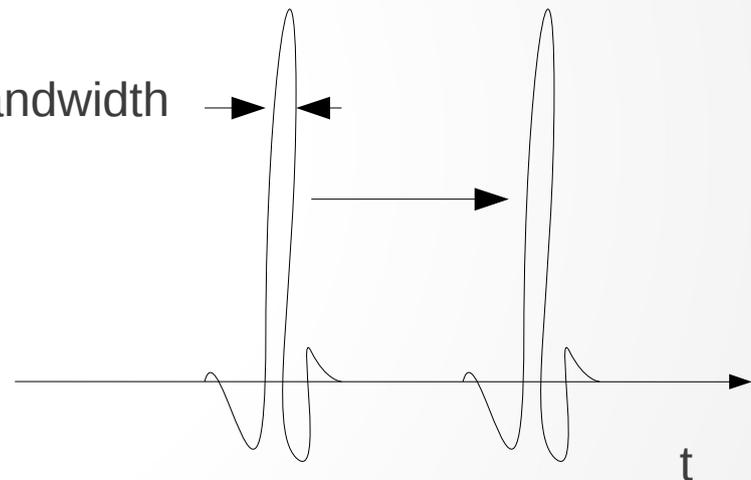


$u(t)$

Civil emitter  
(illuminator of opportunity - non-cooperative)



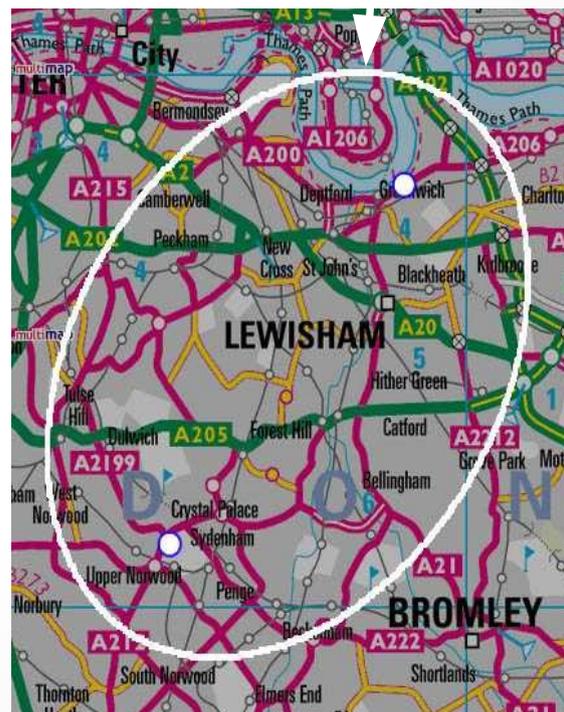
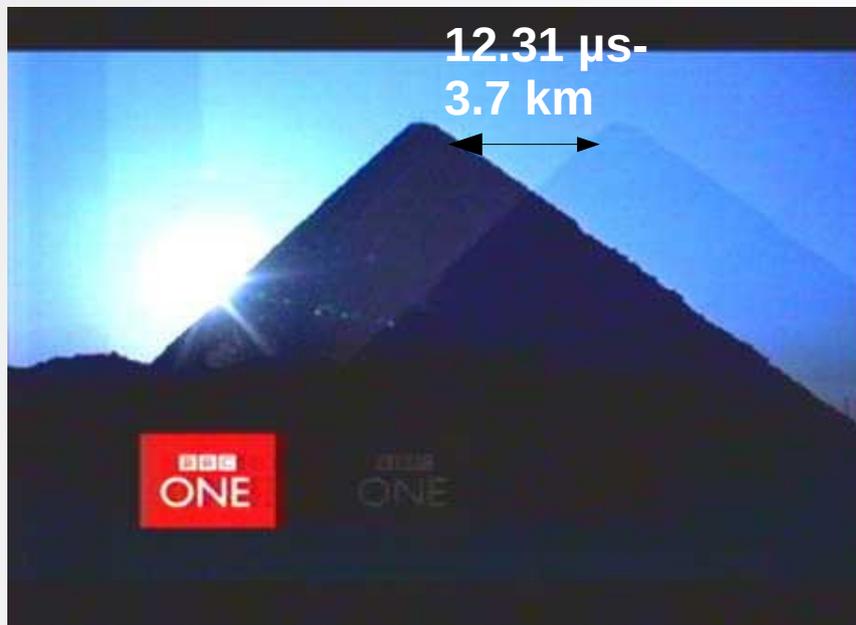
$1/\text{Bandwidth}$



But need to estimate the direct response between the emitter and the receiver

Range resolution  $\sim c_0/B$

# Ghost effect



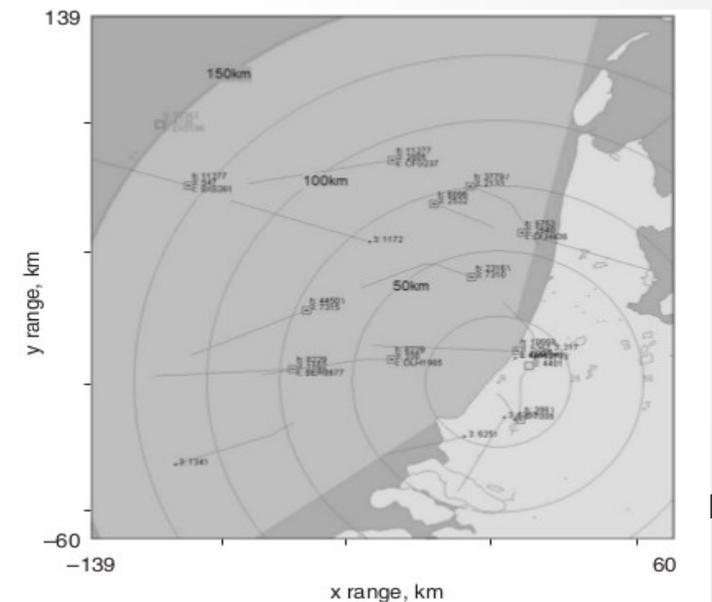
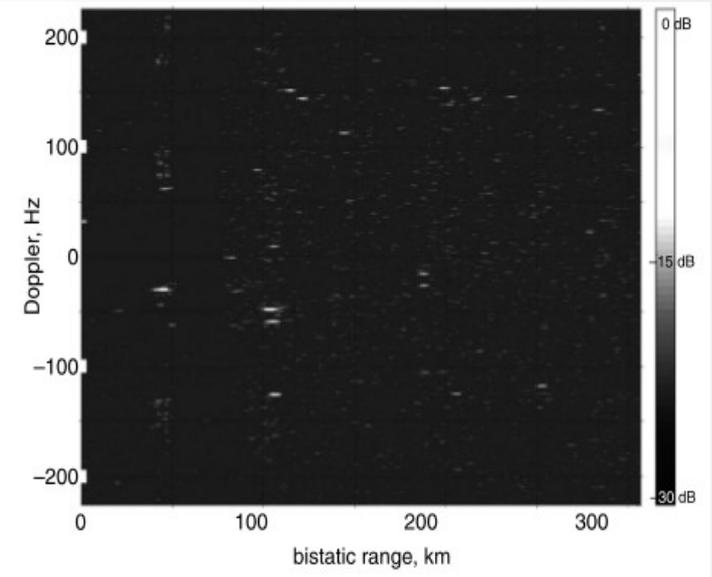
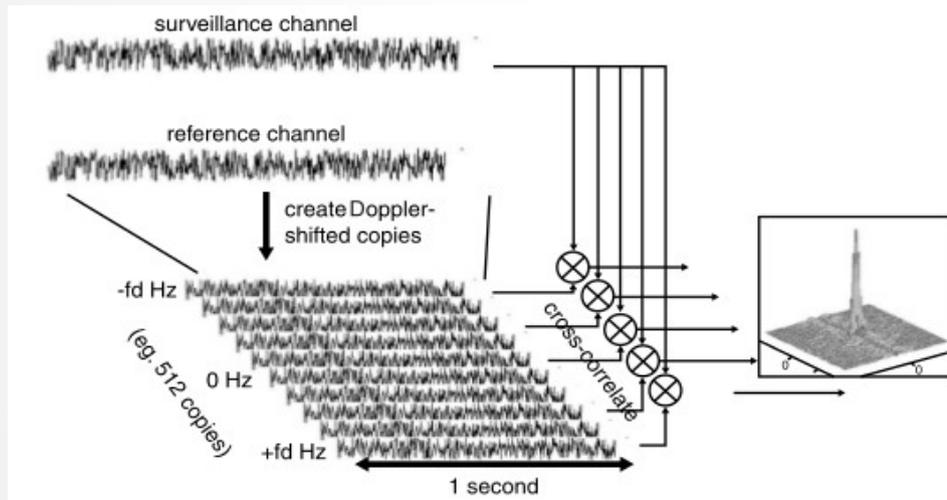
Analog TV  
470-790 MHz  
Reflections on buildings

Source: <http://www.frisnit.com/radar/>

# Application to aircraft detection

PE Howland, D Maksimiuk, G Reitsma - ... -Radar, Sonar and Navigation, 2005 - IET

## Illuminator of opportunity FM emitter



Resolution : 100kHz bandwidth  $\rightarrow$  1.5km

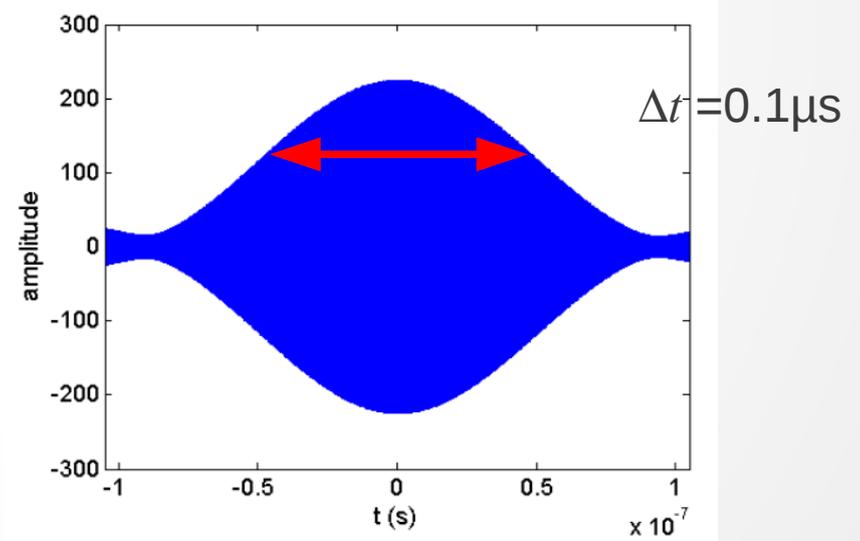
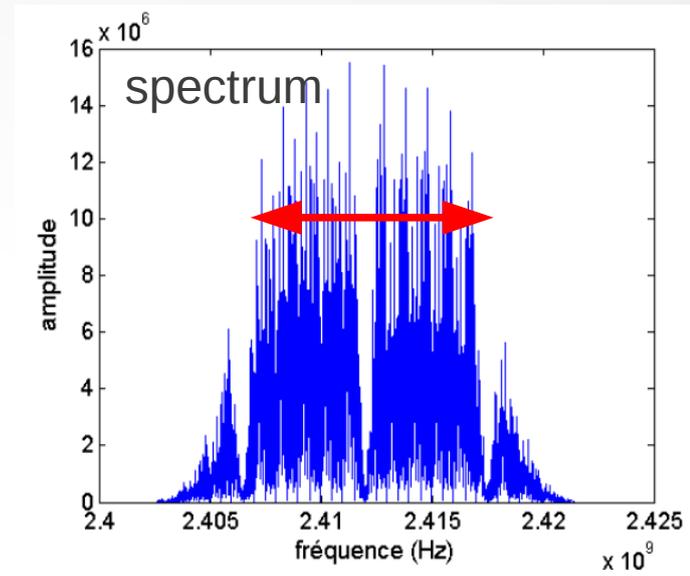
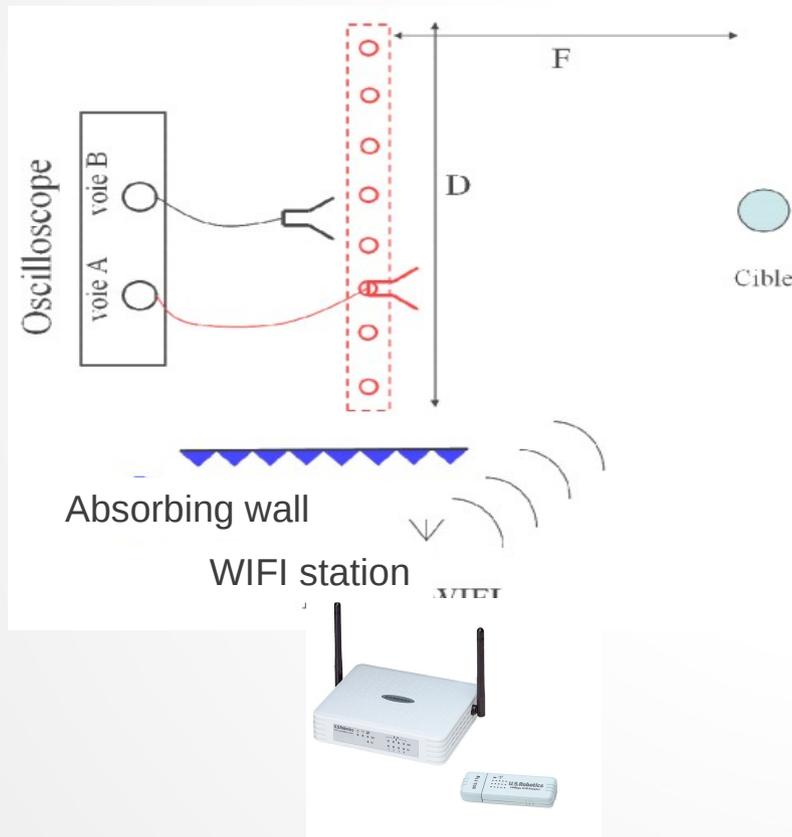
# Multistatic passive RADAR with source of opportunity

# Multistatic passive detection



Horn antennas

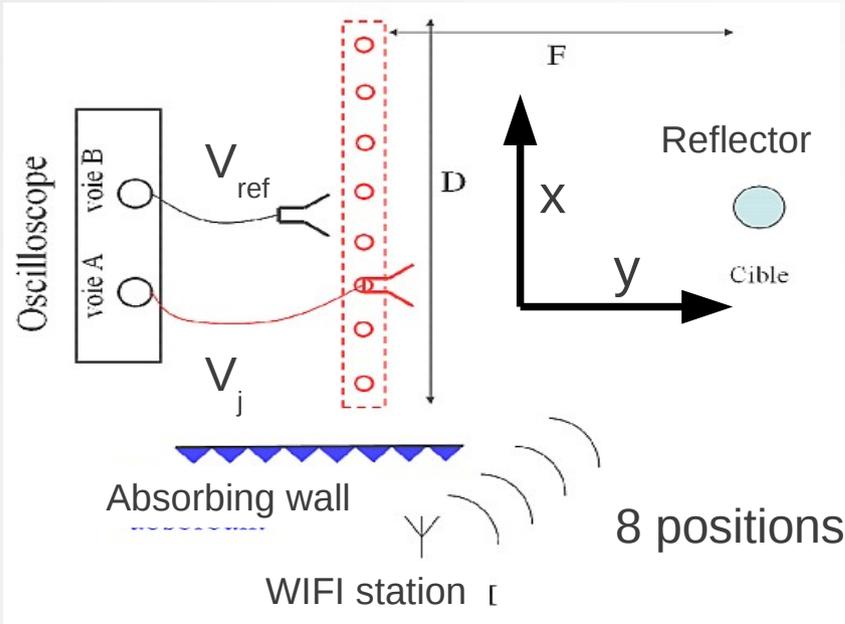
Wide-band –  
directive and  
vertically  
polarized  
antenna



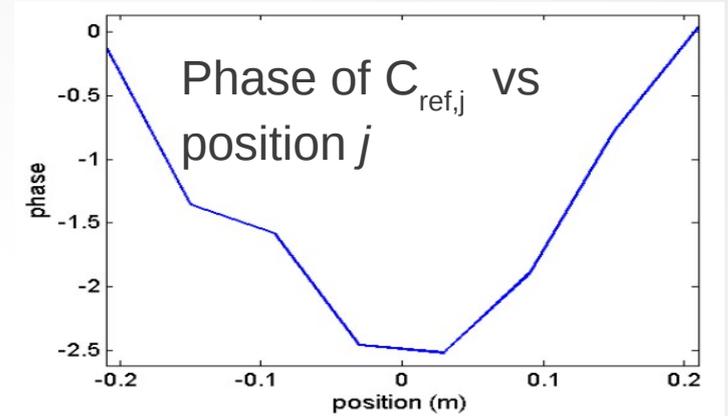
Range resolution :  $\Delta t/2c = 15 \text{ m}$  12

→ Monochromatic detection at indoor scale

# Multistatic passive detection

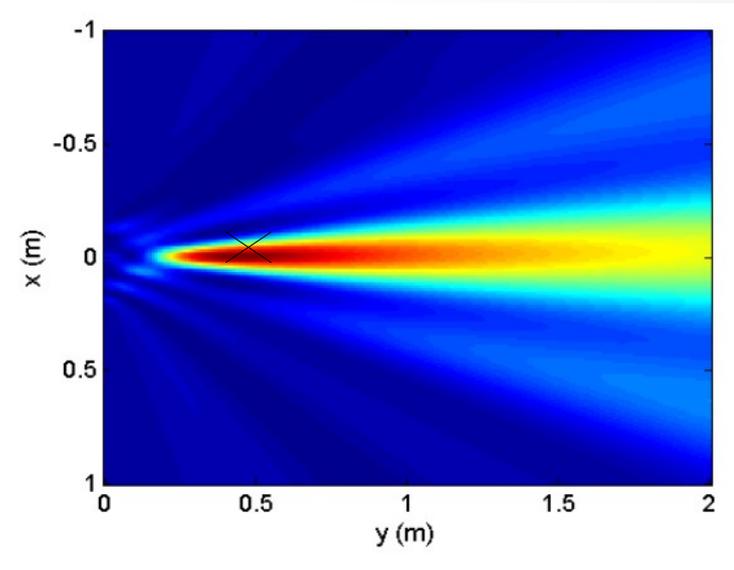


$C_{ref,j} = \langle V_{ref} V_j^* \rangle$   
Cross-correlations  
averaged over  
10000 acquisitions



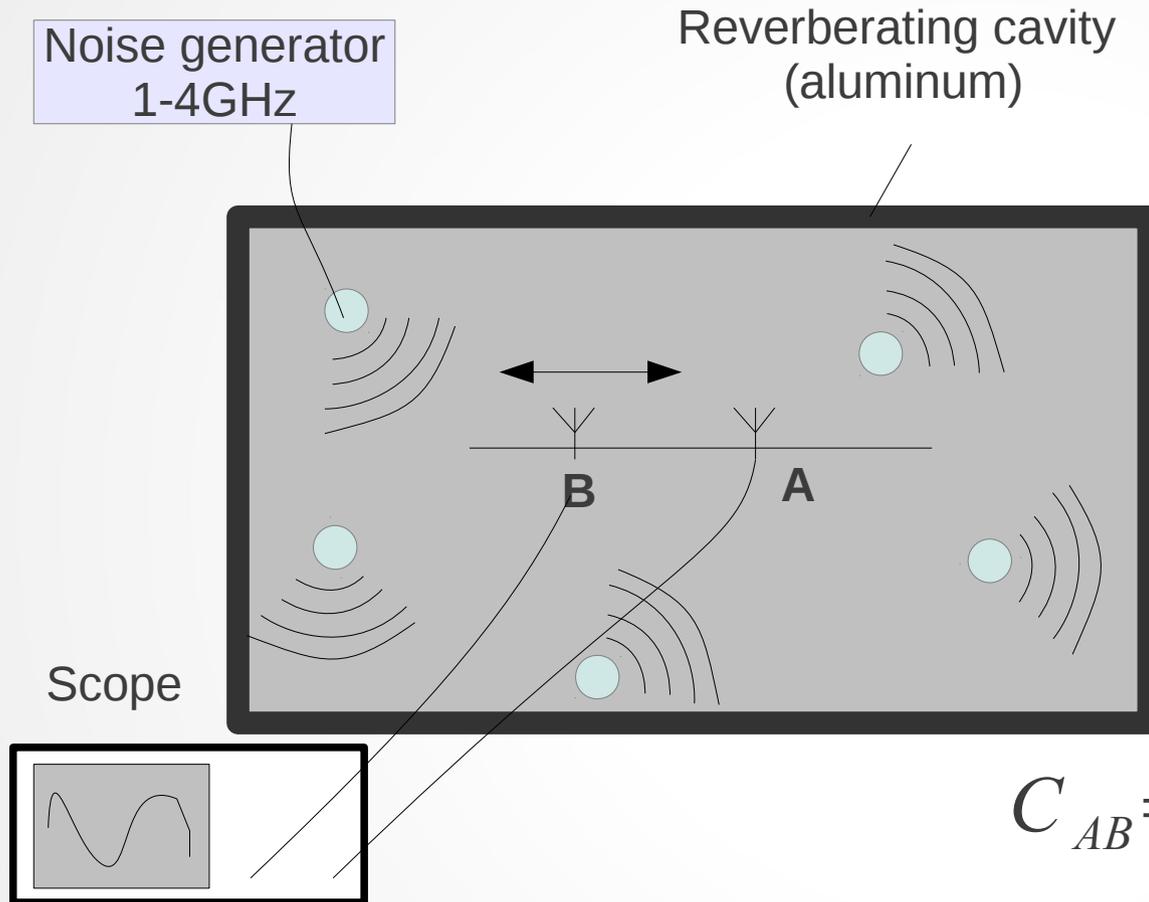
Classical beam-forming

$$I(x, y) = \left| \sum_{\text{positions}} C_{ref,j} \exp(-j k_0 \sqrt{(x - j \delta x)^2 + y^2}) \right|$$



# Wideband diffuse artificial noise

# Correlations in cavity



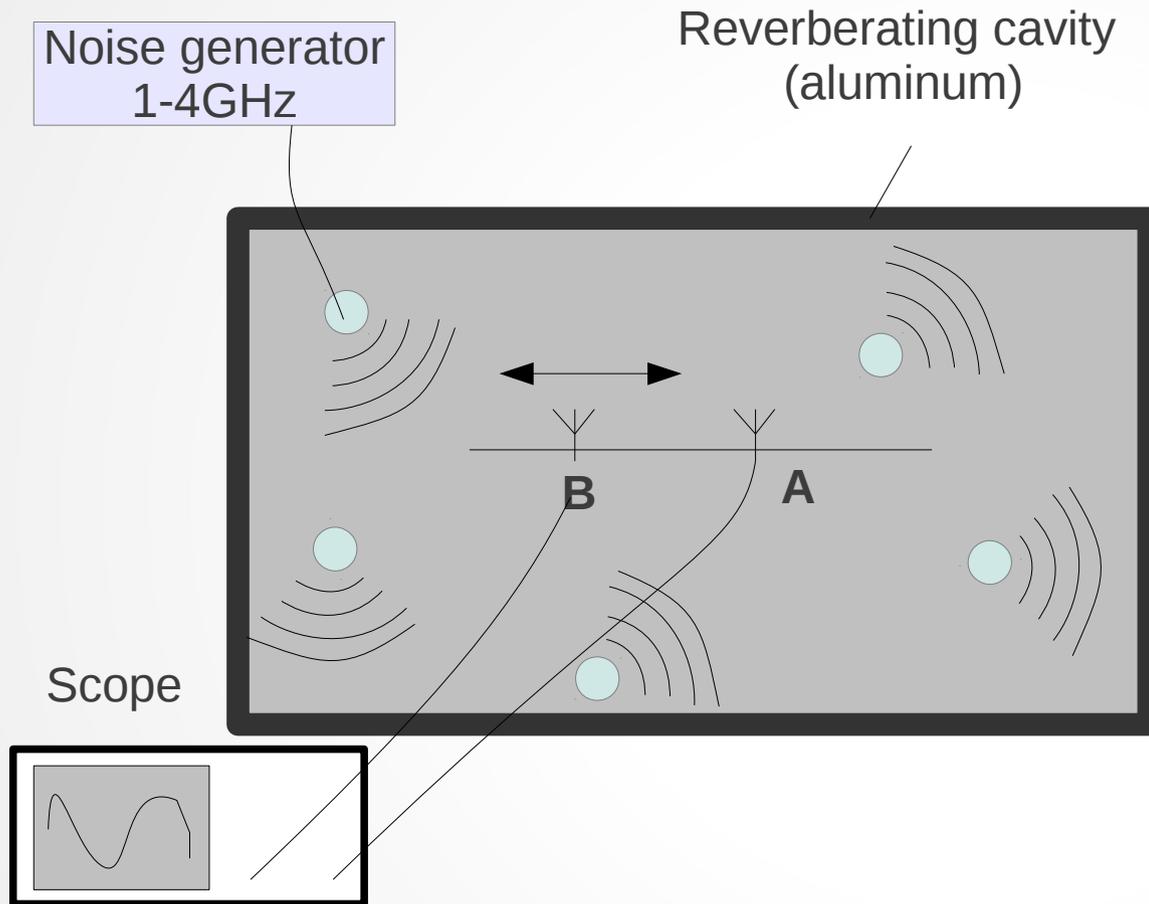
But : coupling between antennas when they are close



$$C_{AB} \neq G(A, B, t) - G(A, B, -t)$$

**Solution?**

# Correlations in cavity



## Correlations of correlation

Antenna A is a fixed reference antenna and we compute

$$C_{BB'} \approx \frac{C_{AB} C_{AB'}}{C_{AA}}$$

Fourier domain

Inverse Fourier transform

# Setup

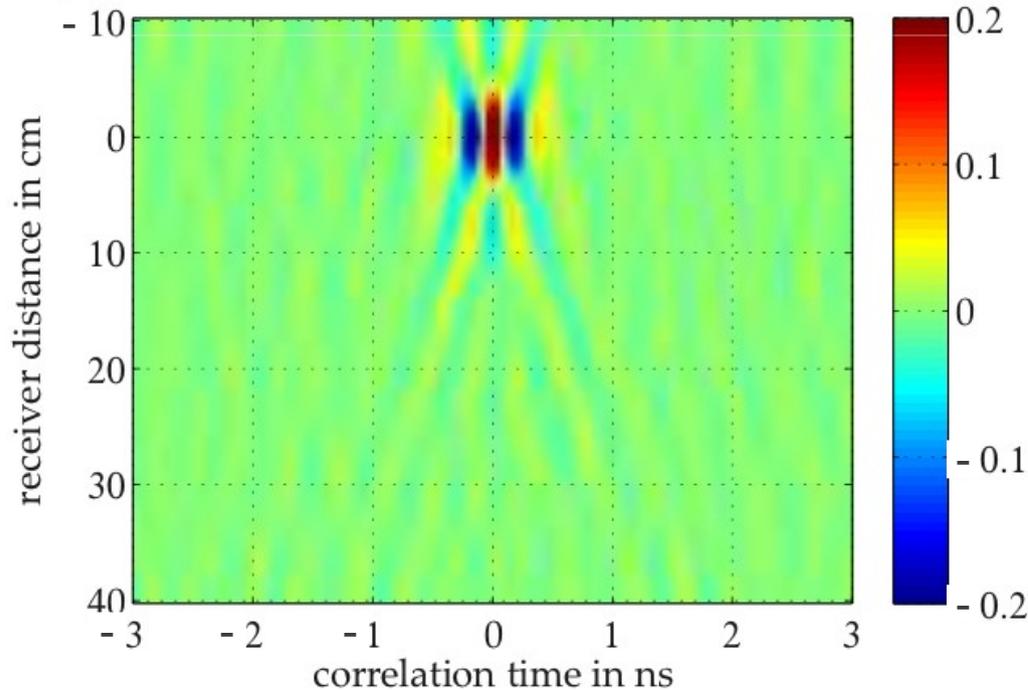


**Reverberation cavity** used in experimental set-up containing an **elliptic mirror** as a reflector, **emitting dipole** and horn **antennas (1-6)**, a **stationary receiver antenna (A)** and a **moving receiver (B)**; MIMO switch allows for successive emission from sources

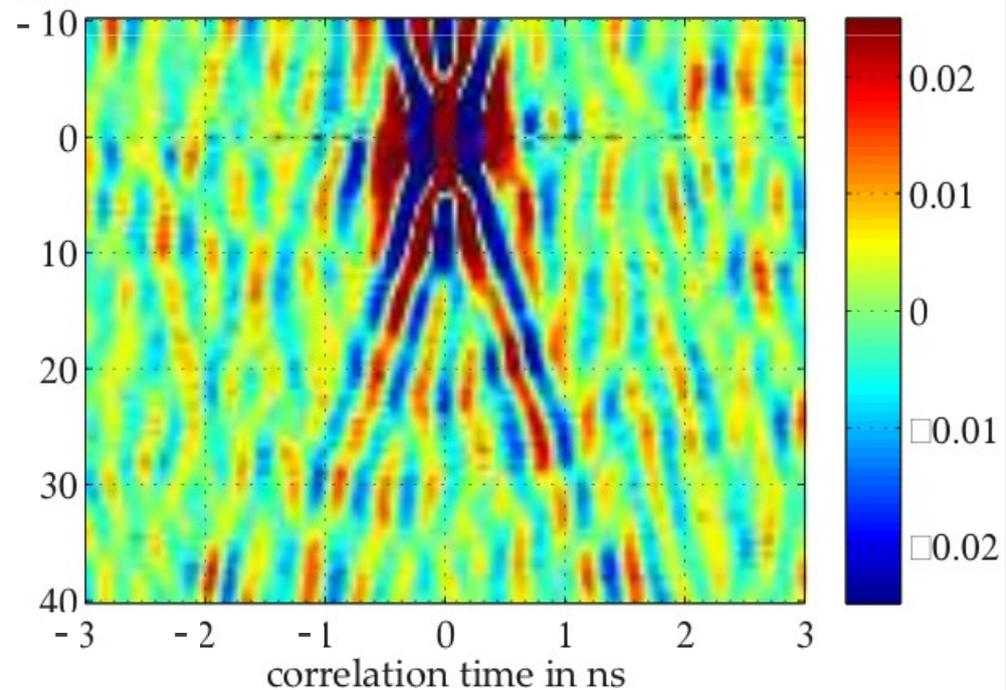
# Empty chamber

- With **6 noise sources**
- “**correlation of correlation**” technique
  - Zero “antenna distance” possible
  - Less noise
- clearly **symmetric** around  $t=0$  until  $d=30$  cm

(a) full amplitude range

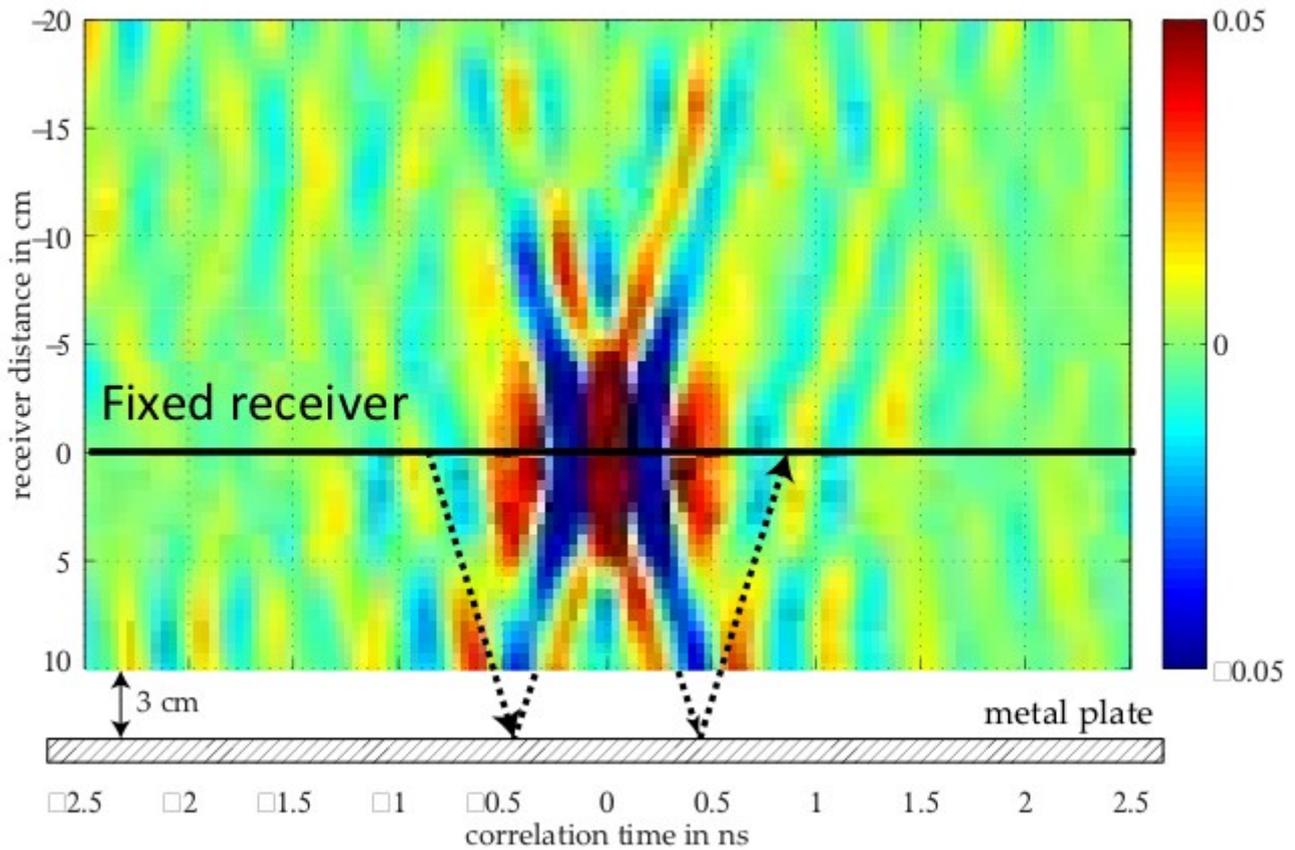
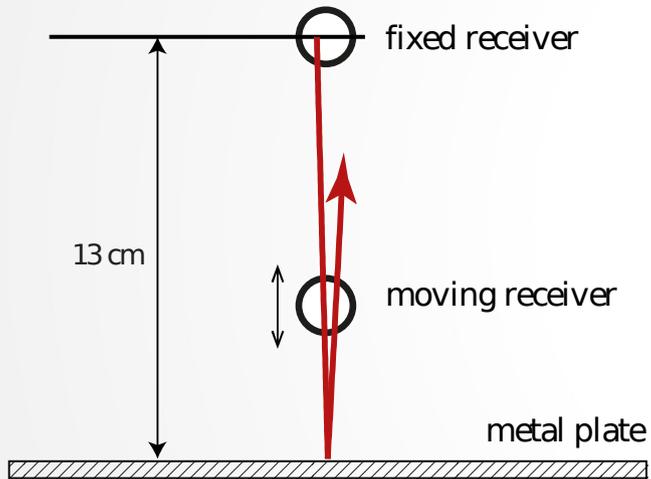


(b) limited amplitude range



# Plate reflector

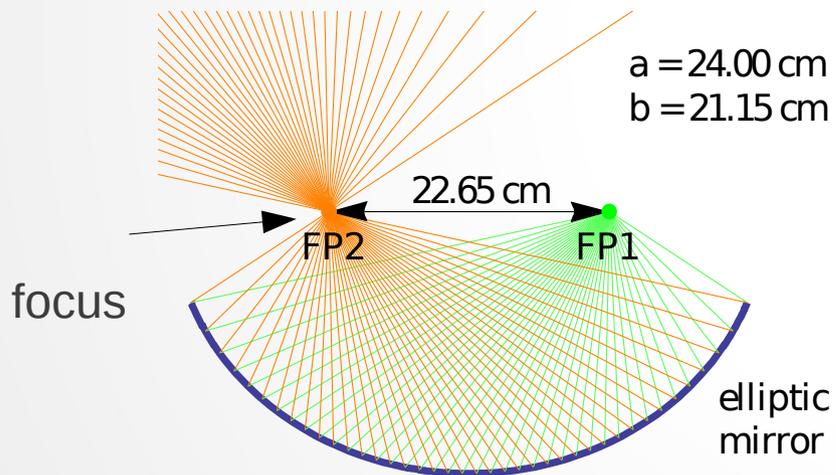
## Reflective metal plate



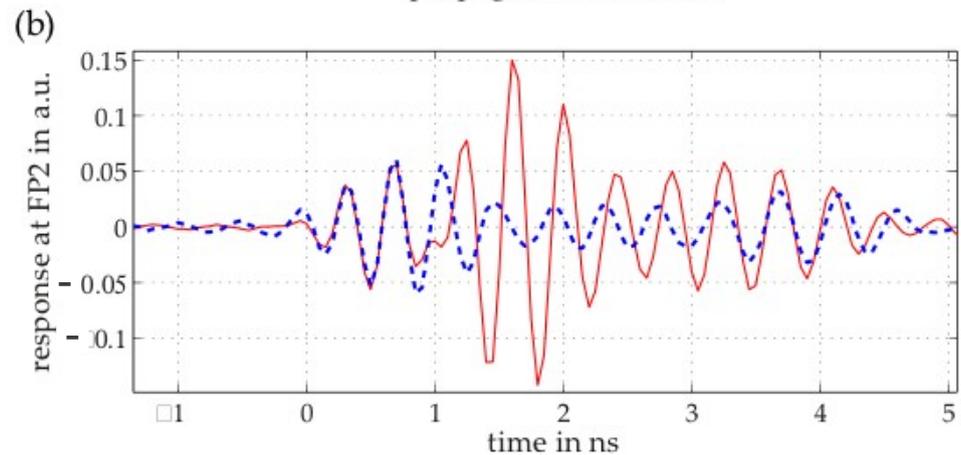
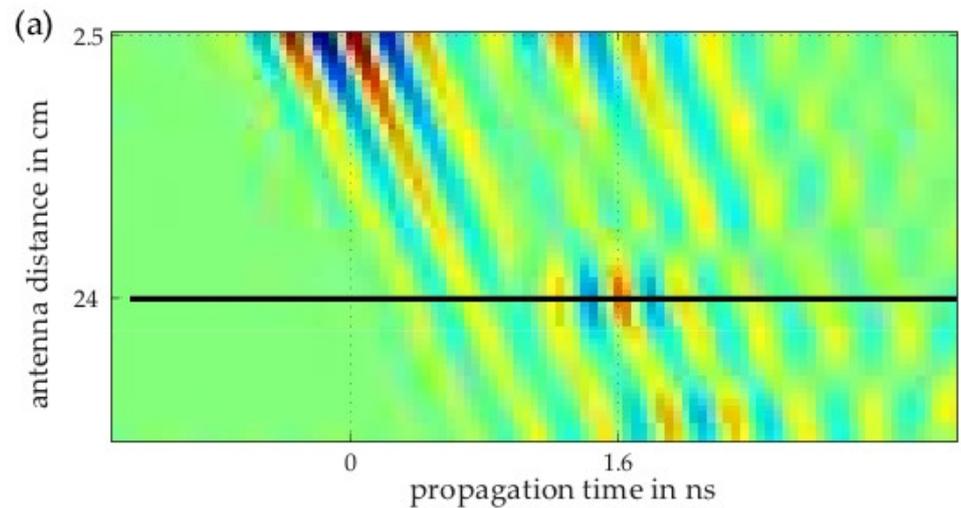
# Elliptic reflector

## Elliptic mirror

- Energy from focal point FP1 is refocused on FP2
- Strong “signature” in Green’s function

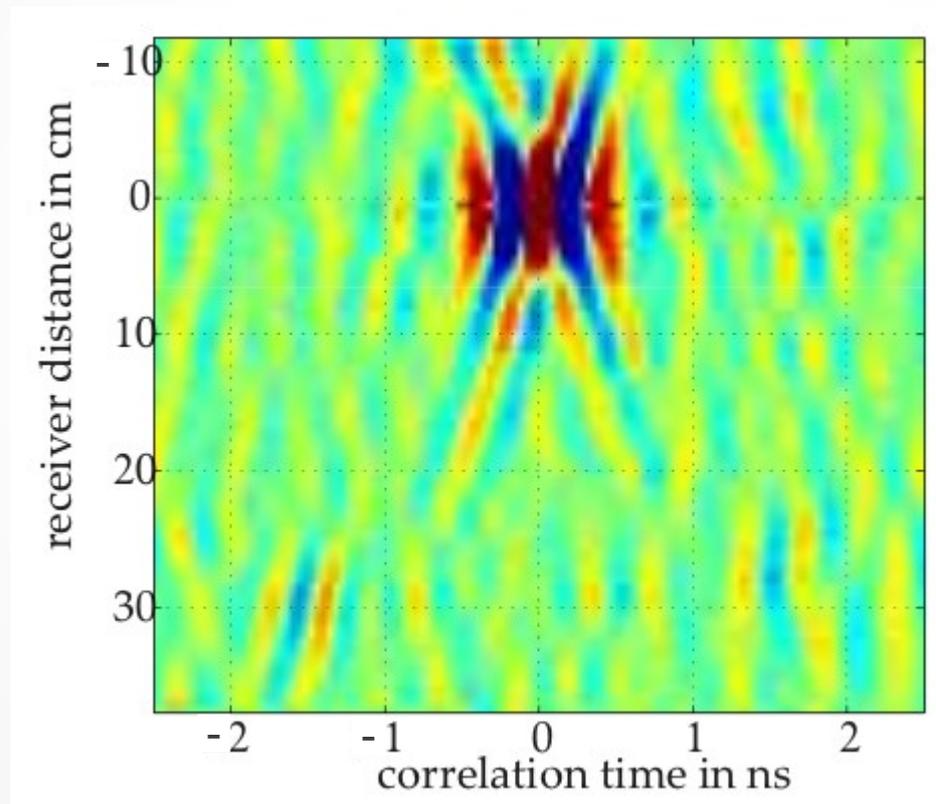


## Active emission from FP1



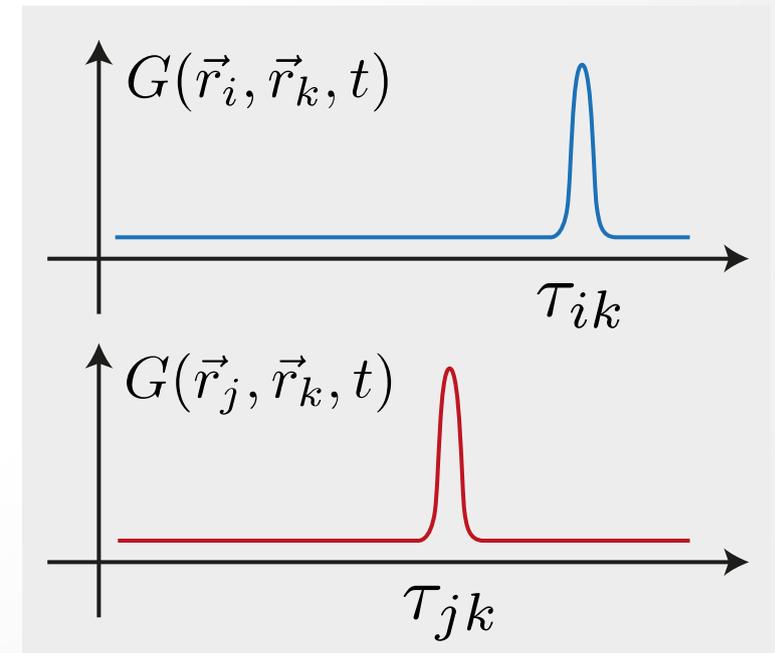
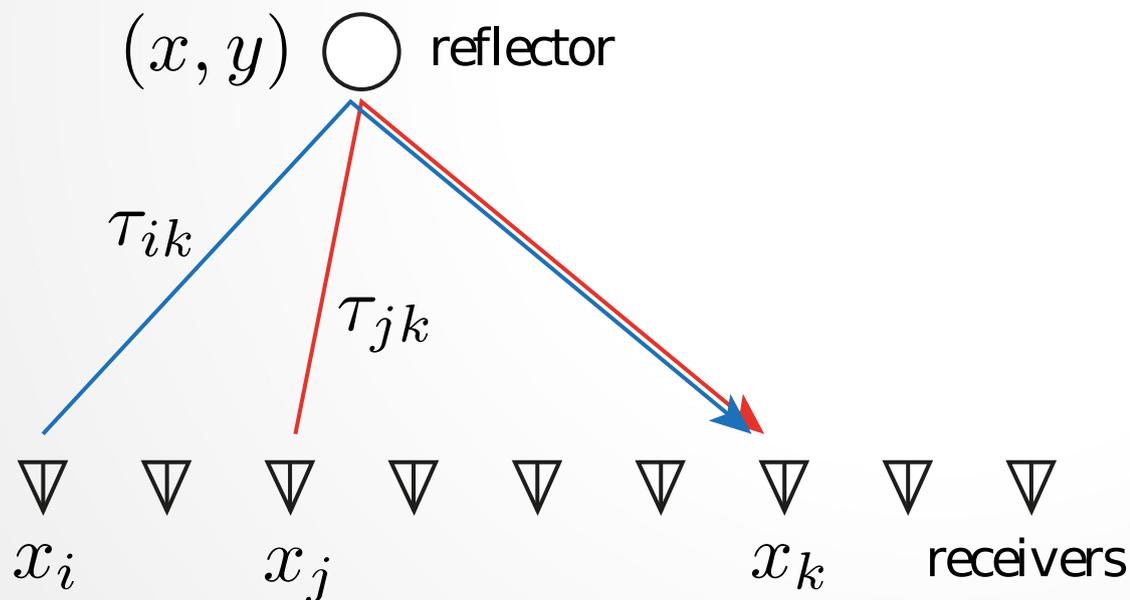
# Elliptic reflector

- One reference point placed on focal point
- reflection around  $d=25$  cm (2nd focal point) visible after 1.7 ns



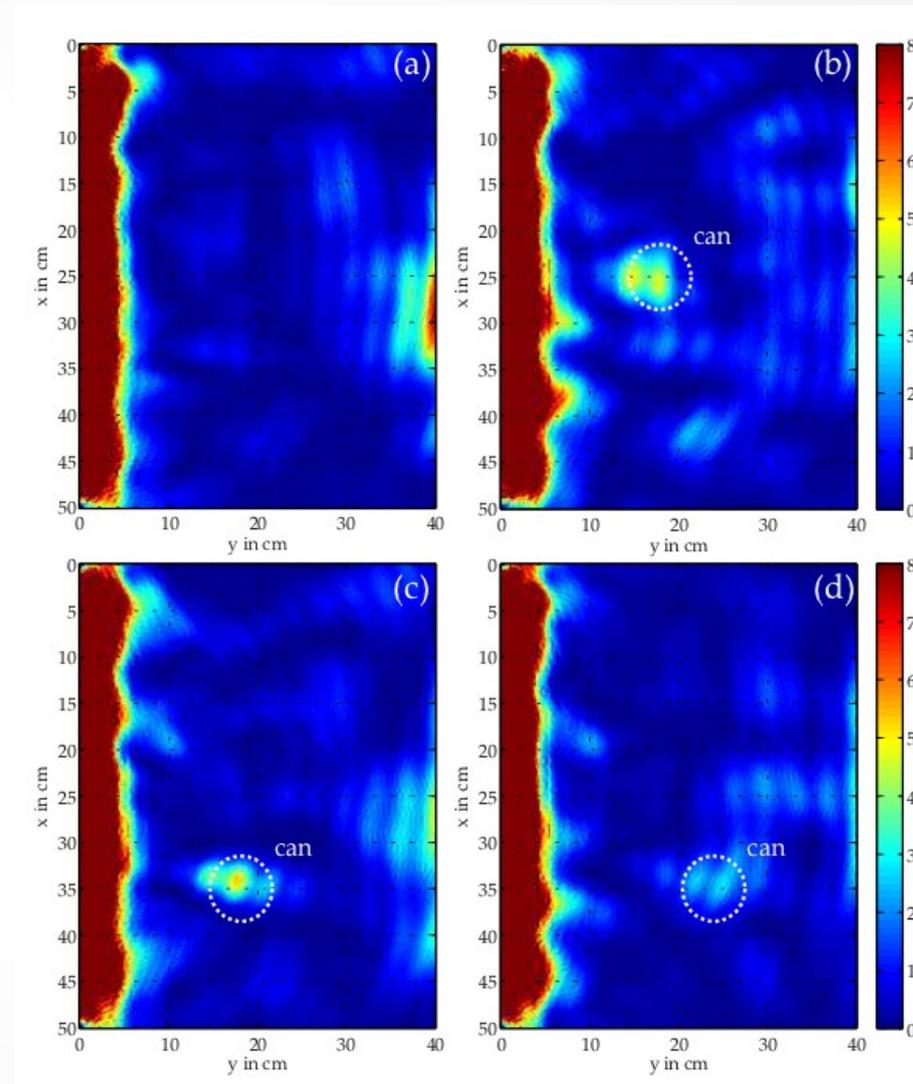
# Beamforming

- Goal: **find reflectors** (on a map)
  - Noise cross-correlation gives access to **impulse responses between virtual transducers**
  - Suggest a reflector for every point on a plane
  - **Delay** the recovered GFs **by the theoretical travel time**
  - Integrate around  $t=0$



# Detection of a metal can

- (a) empty cavity
- (b-d) different locations
- Better quality for small distances from transducer array
- Distorted by reflections from cavity wall at  $y = 40$  cm
- **Compensate for lack of noise isotropy** by making use of the causal AND anti-causal part of the GF



# Thermal correlations

# In acoustics

VOLUME 87, NUMBER 13

PHYSICAL REVIEW LETTERS

24 SEPTEMBER 2001

## Ultrasonics without a Source: Thermal Fluctuation Correlations at MHz Frequencies

Richard L. Weaver and Oleg I. Lobkis

*Theoretical & Applied Mechanics, University of Illinois, Urbana, Illinois 61801*

(Received 5 April 2001; published 7 September 2001)

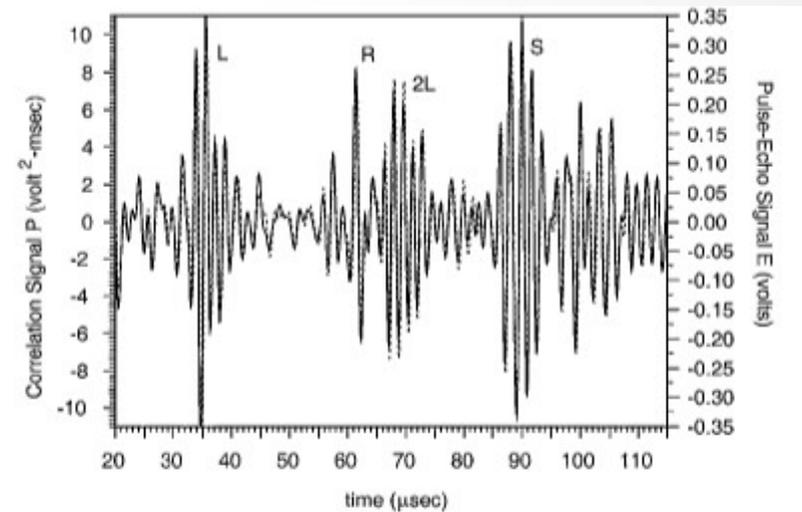
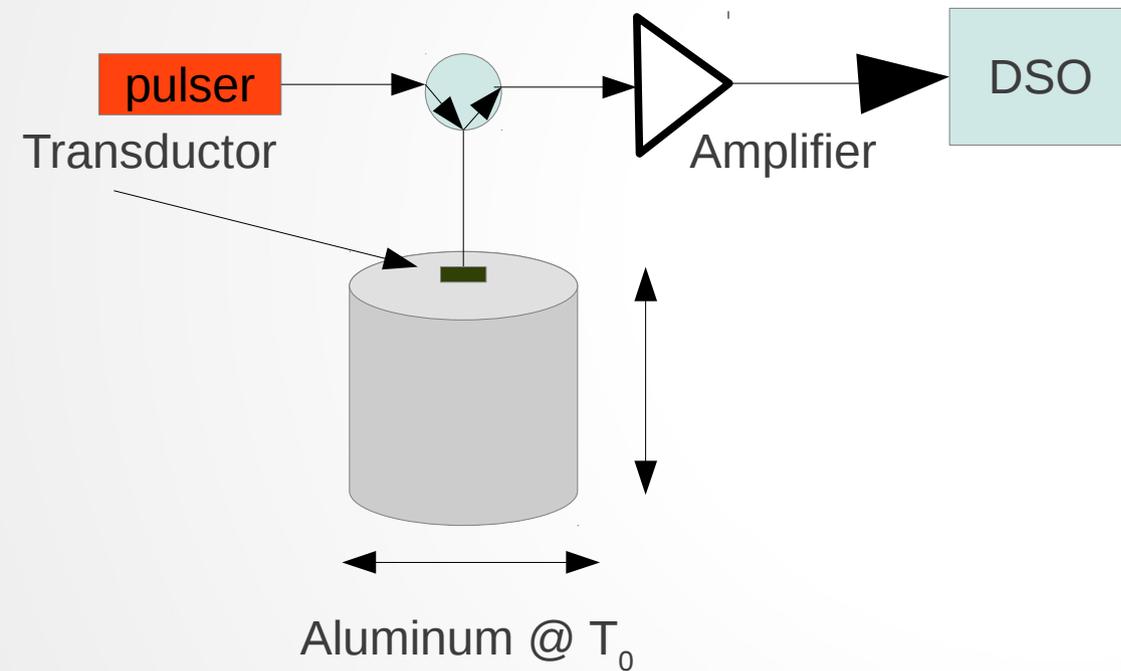


FIG. 2. Comparison of the noise autocorrelation function  $P$  (solid line) and the direct pulse/echo signal  $E$  (dotted line). They

Elastic waves

Active measurement

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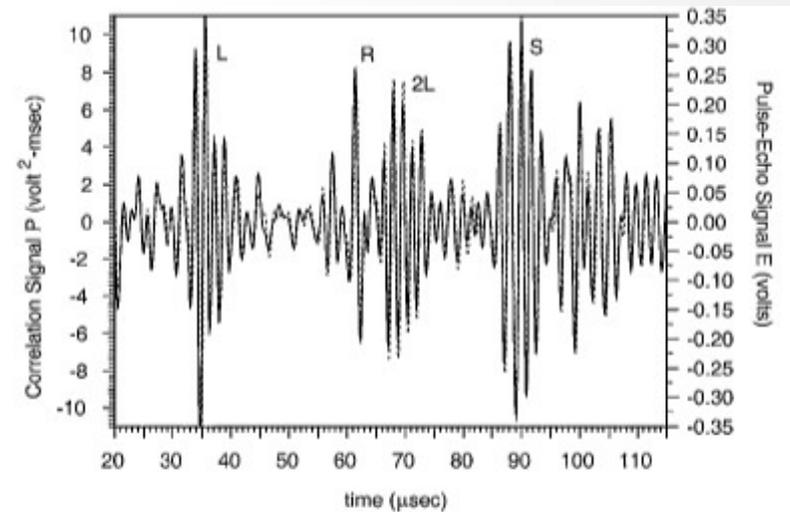
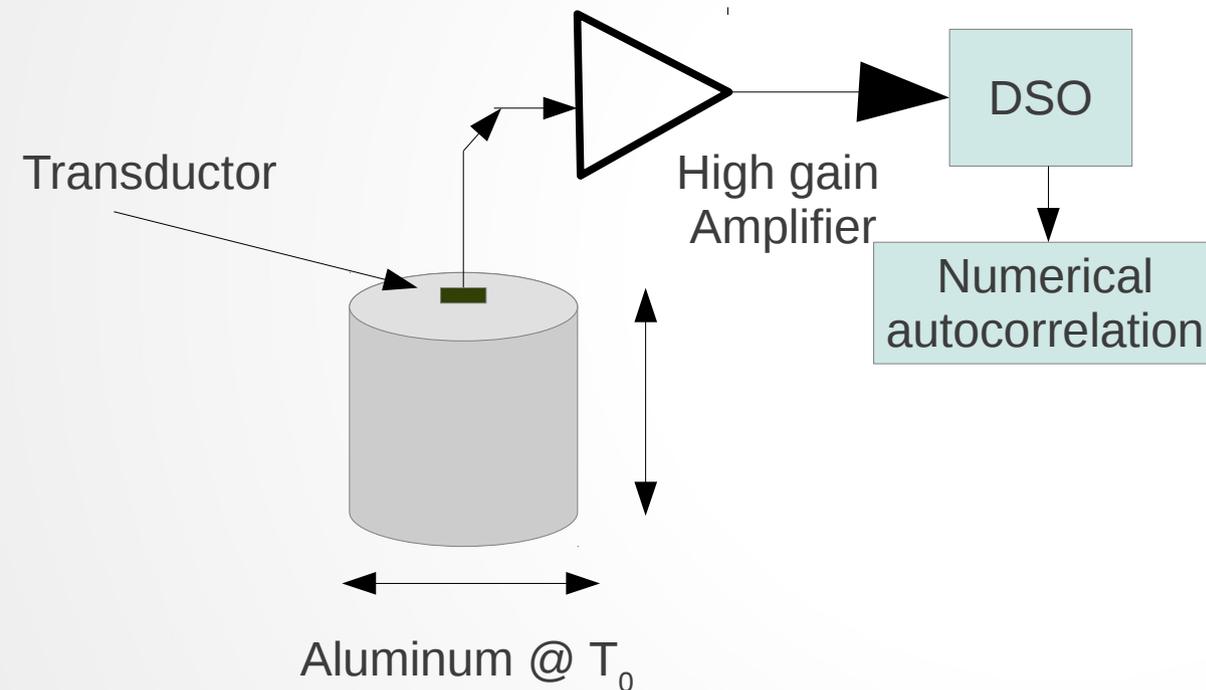


FIG. 2. Comparison of the noise autocorrelation function  $P$  (solid line) and the direct pulse/echo signal  $E$  (dotted line). They

Elastic waves

Passive measurement

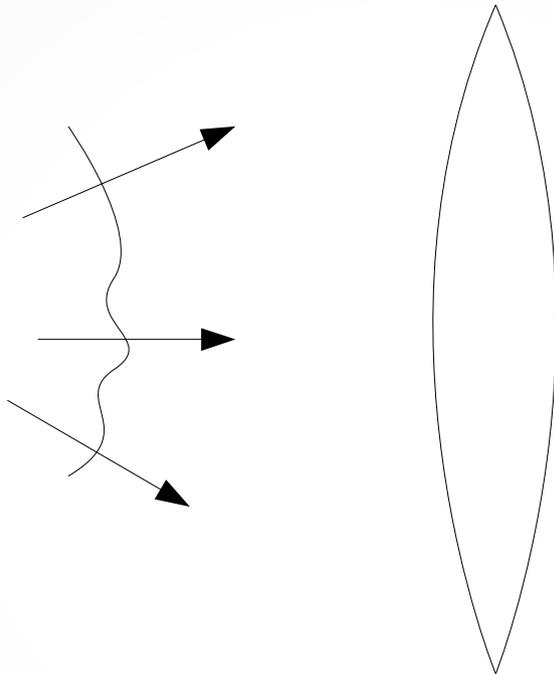
$\text{Im } G(A,A)$  recovered from thermal phonons<sup>27</sup>

# IR camera

Thermographic camera



Hot system  
emits thermal  
radiation



Lens

$\lambda \sim 9 - 14 \mu\text{m}$



Mean intensity  
distribution

Source: NASA

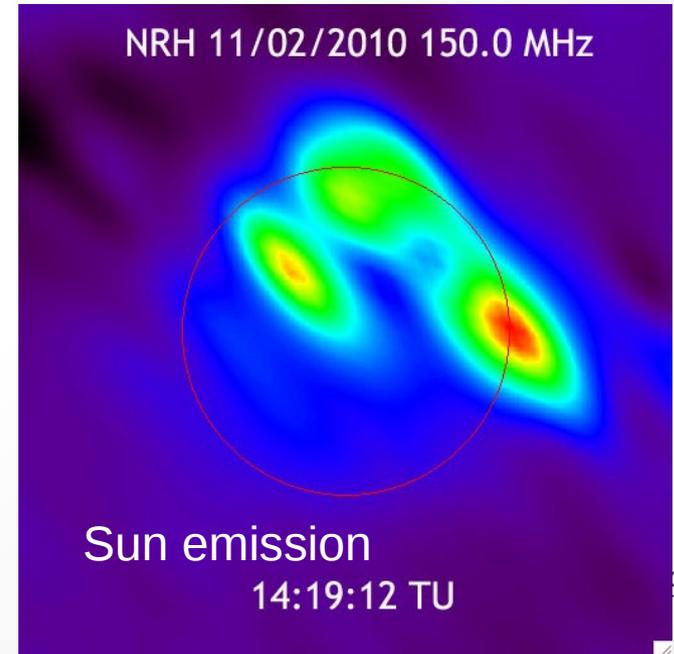
# Interferometric arrays

: 47 antennas, frequencies : 150  
- 450 MHz

Radio telescope



Beamforming



Source : Station de Radioastronomie de Nançay

# Black body radiation

Black body radiation at temperature T

## Planck's law

$$B(T, \nu) = \frac{2h\nu^3}{c^2} \frac{1}{\exp\left(\frac{h\nu}{k_b T}\right)}$$

Spectral radiance (W/m<sup>2</sup>/sr/Hz)      Boltzmann constant

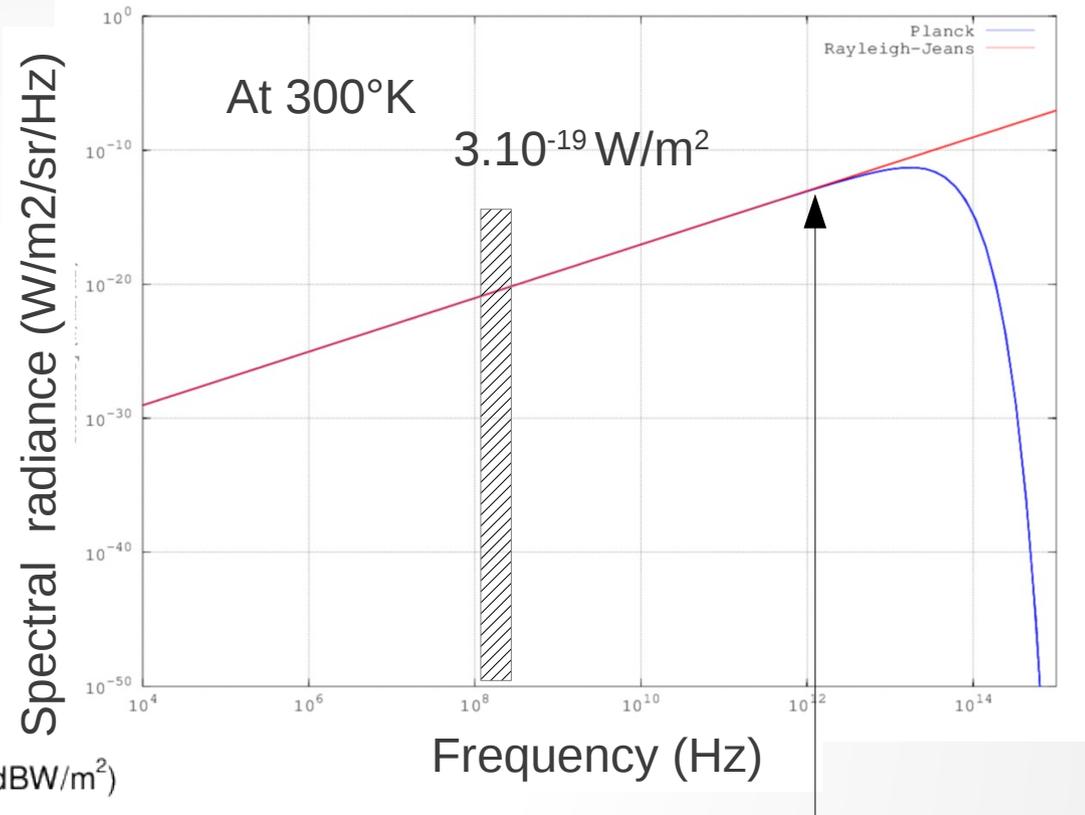
$$h\nu \ll kT \quad B(T) \approx \frac{2k_b T \nu^2}{c^2}$$

Rayleigh-Jeans  
classical limit

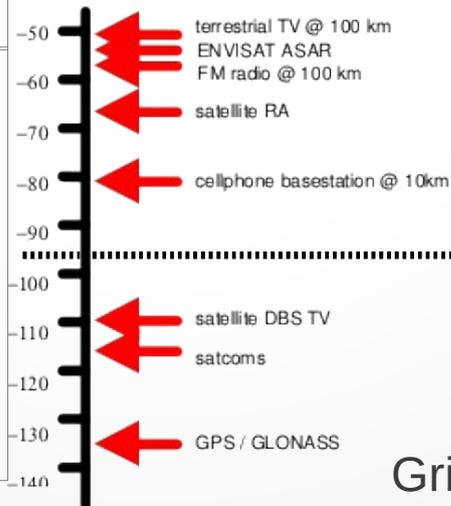
$$I(T) \approx \frac{8\pi k_b T \nu^2}{c^2} \delta\nu$$

T=300K Δf=10MHz, ν=2GHz

→ I(T)=-103 dBW/m<sup>2</sup>



Φ (dBW/m<sup>2</sup>)

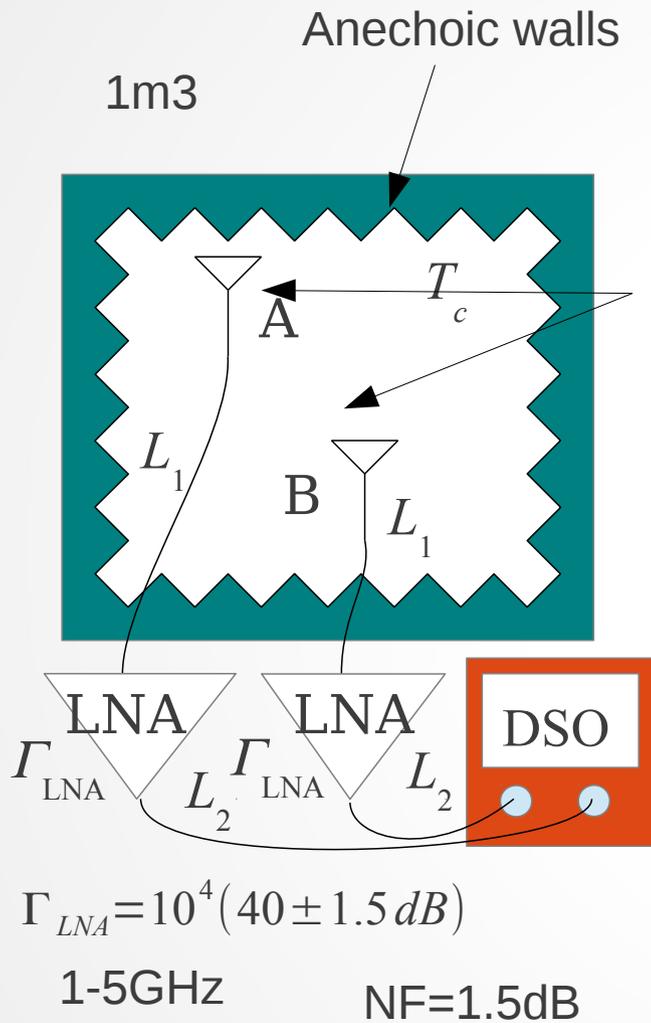


$\nu \sim 6.62\text{THz}$  ( $\lambda \sim 45\mu\text{m}$ )

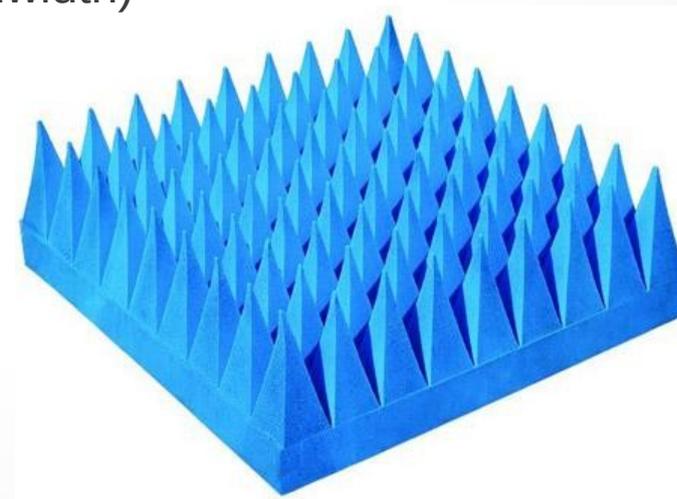
Thermal noise at  
microwave range  
can be measured

Griffiths

# Experimental set-up



Omnidirectional  
(50Ω, 2.5dBi gain  
1-5GHz  
bandwidth)



Absorbing material

# Absorbing cavity $\leftrightarrow$ blackbody

THE REVIEW OF SCIENTIFIC INSTRUMENTS

VOLUME 17, NUMBER 7

JULY, 1946

## The Measurement of Thermal Radiation at Microwave Frequencies

R. H. DICKE\*

*Radiation Laboratory, Massachusetts Institute of Technology, Cambridge, Massachusetts\*\**

(Received April 15, 1946)

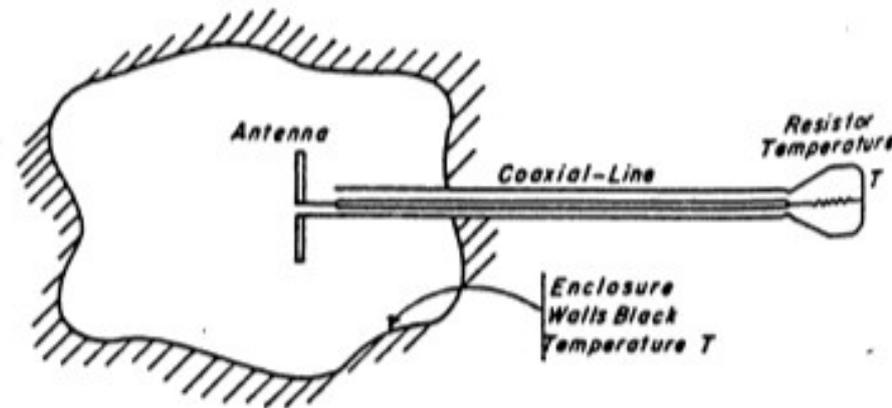


FIG. 1. Antenna system in black enclosure.

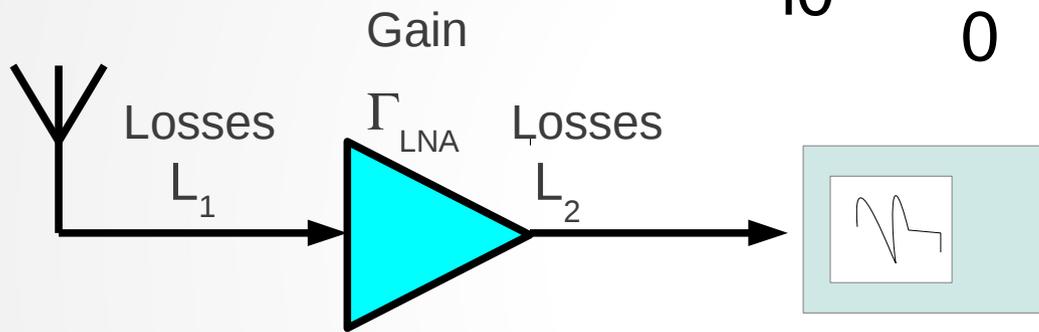
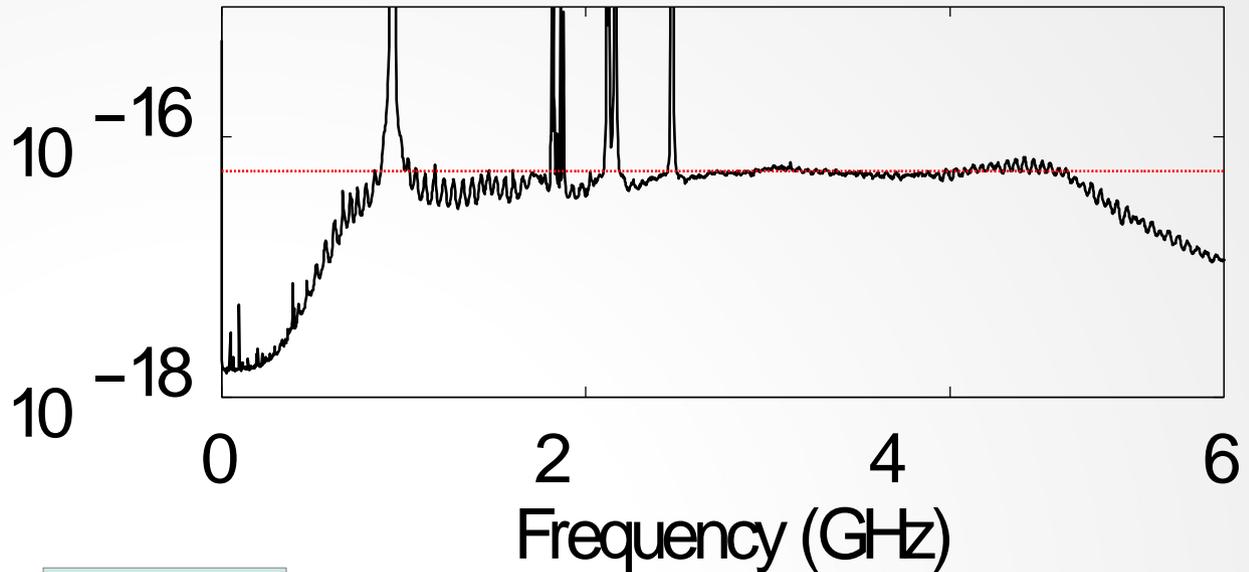
Perfect blackbody cavity : at thermal equilibrium power spectral density(PSD)  $=k_b T$

# Power spectral density in the cavity

$$N = \frac{\langle |U(\omega)|^2 \rangle}{Z_0}$$

Average over 40000 acq.

W/Hz



4 main sources of noise :

- $N_a$  : microwave noise
- $N_{lna}$  : Low noise amplifier
- $N_c$  : Losses in coaxial cables
- $N_s$  : Noise of the scope

$$N_a = \epsilon k_B T_c L_1 L_2 \Gamma_{LNA}$$

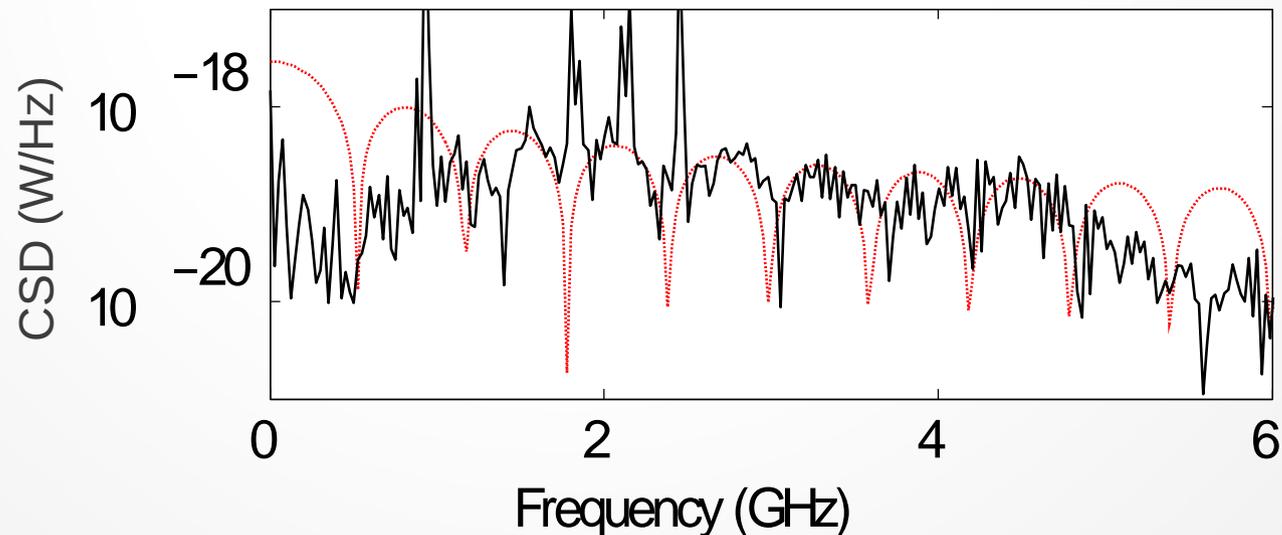
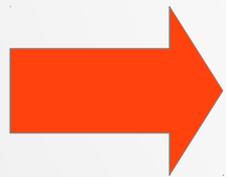
$$N_{LNA} = k_B T_{LNA} L_2 \Gamma_{LNA}$$

$$N_c = k_B T_c \left( 1/L_1 - 1 \right) L_1 L_2 \Gamma_{LNA}$$

$$N = N_a + N_{LNA} + N_c + N_s$$

# Process

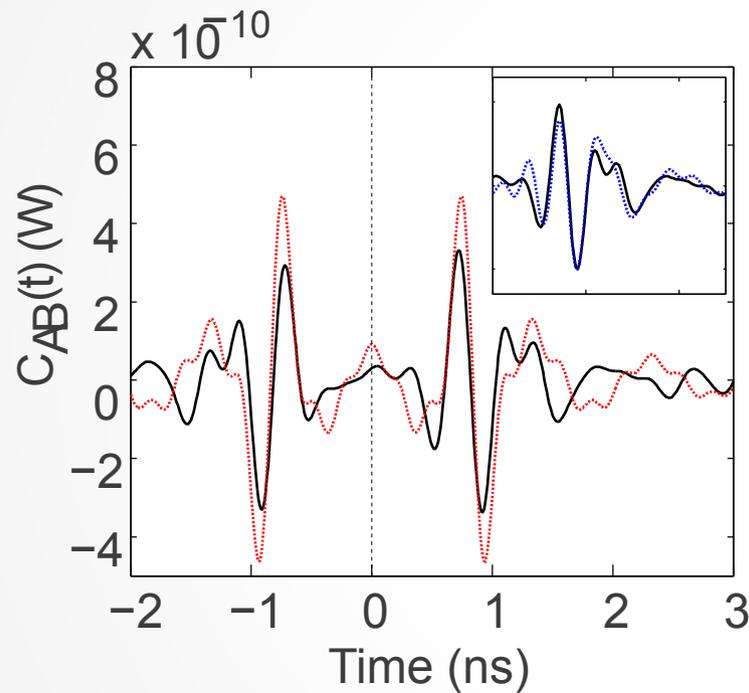
- 50,000 acquisitions of 40ns long signals for each channel
- Fourier transform over the 2x50,000 acquisitions
- $C_{AB}(\omega)$  cross-spectral density is estimated from the average of the product of the 50,000 Fourier transforms



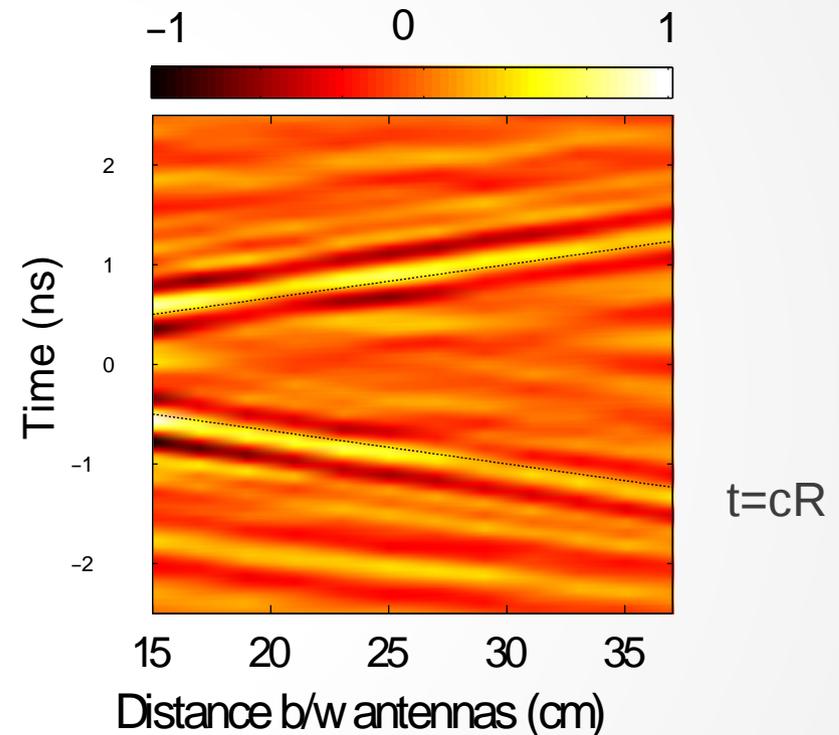
# cross-correlations

Suppression of strong contributions (artificial noise sources) > a few kT  
Fourier transform of the cross-spectral density  $\leftrightarrow$  cross-correlation

Cross-correlations



- Cross-correlations
- FD theorem
- Active direct measure of transient response



$c \sim 3e8$  m/s

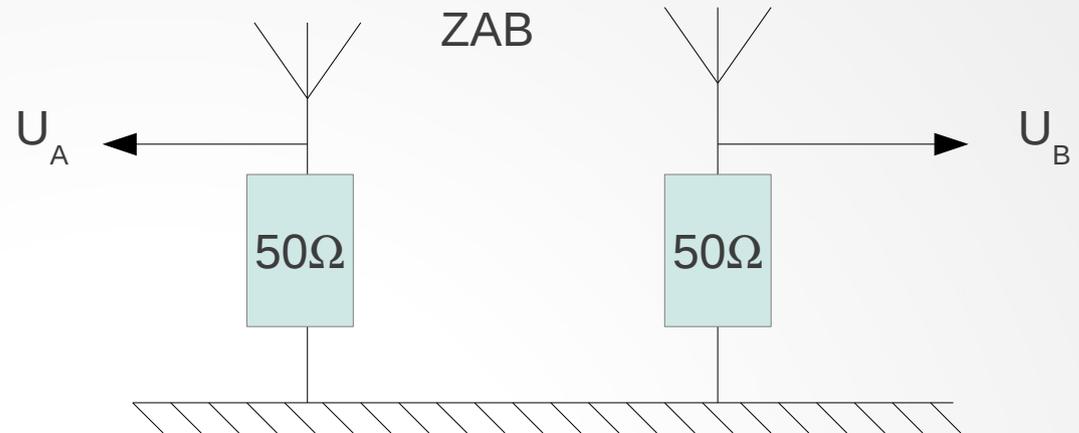
$\rightarrow$  Recovering of the Green's function

# Theoretical correlations

From the scope point of view : electrical problem

Modeling with impedances (linear system)

Fluctuation dissipation theorem applied to  $\mathbf{U}=\mathbf{Z}\mathbf{I}$



$$C_{AB}(\omega) = \frac{\langle U_A U_B^* \rangle}{Z_0} = kT \frac{2 \Re(Z_{AB})}{Z_0}$$

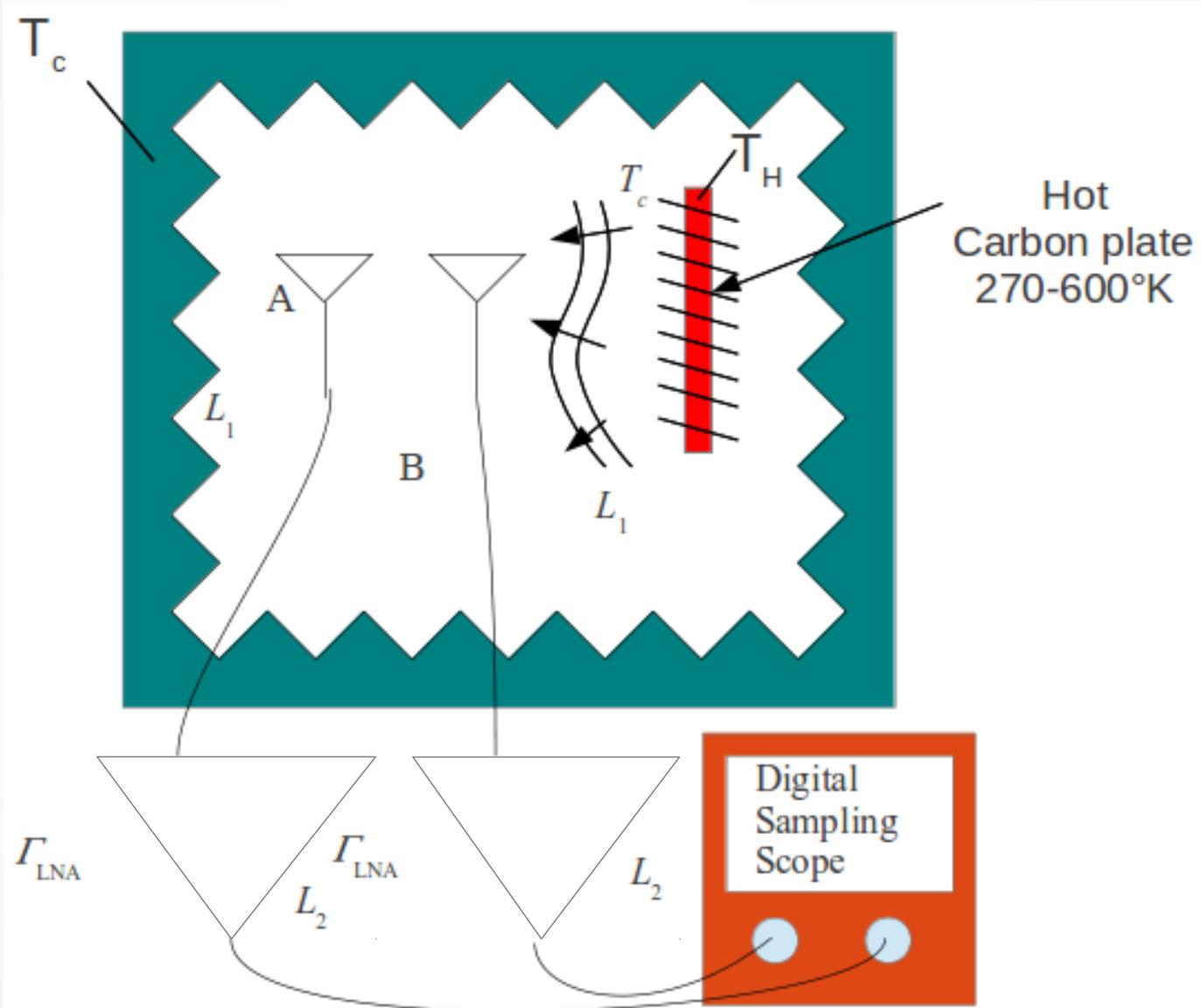


In case of dipole like antennas that are adapted ( $Z_{AA} \sim Z_0$ ), it comes

$$C_{AB}(\omega) = \alpha \Gamma_{LNA} L_1 L_2 \epsilon k_B T_c \frac{3}{2} \left( \sin(k_0 d) \left( \frac{1}{k_0 d} - \frac{1}{(k_0 d)^3} \right) + \cos(k_0 d) \frac{1}{(k_0 d)^2} \right)$$

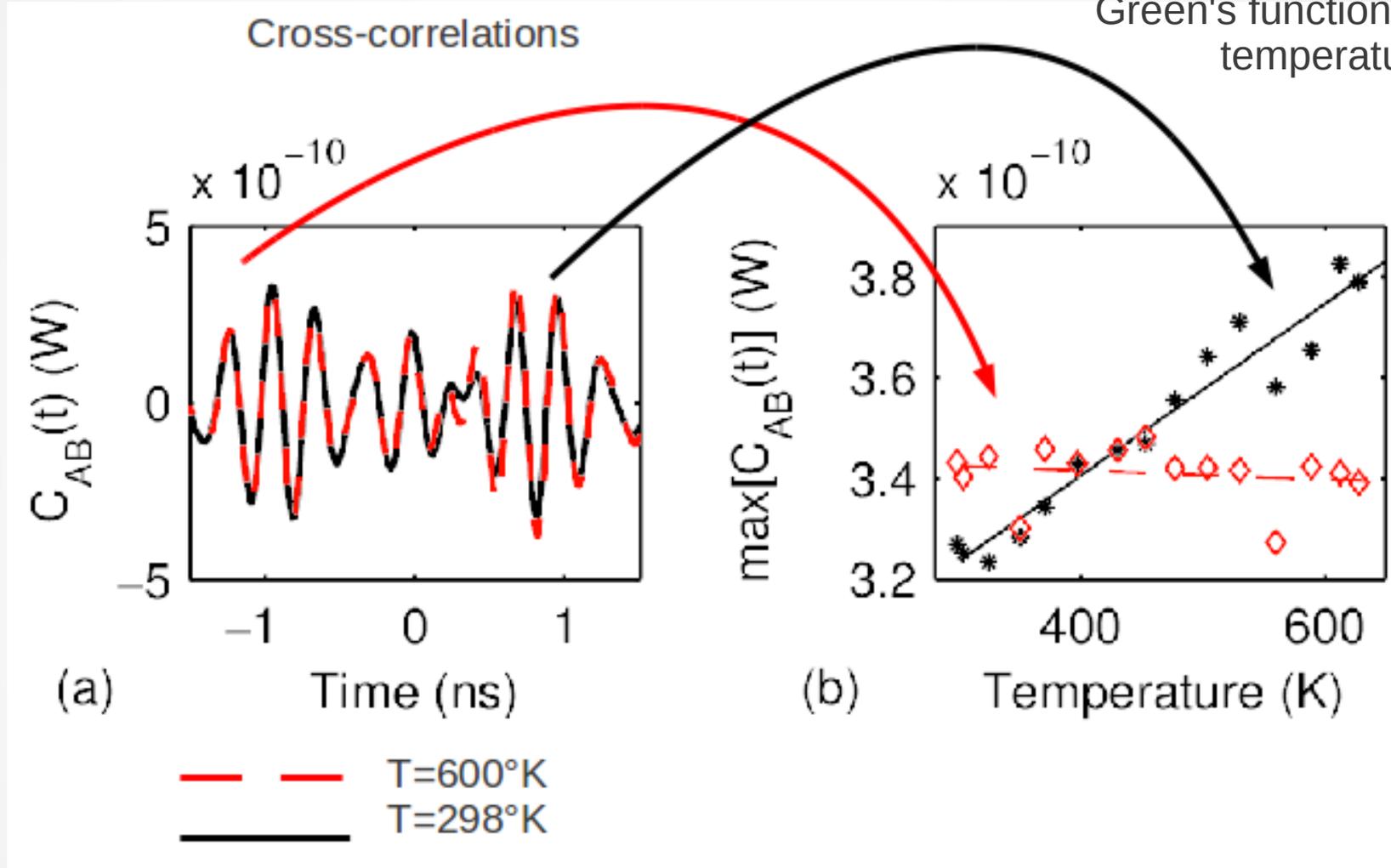
Good fitting with the experimental results

# Hot source



# Measurement results

Maximum amplitude of the causal and anticausal Green's function vs. Plate temperature



**Causal response increases with temperature because the heater increase the thermal flux in one direction**

# Result interpretation

A perfect absorber is a perfect black body

Absorptivity

$\alpha$

Emissivity

$\epsilon$

$$I = I_t + I_e$$

$$I \propto (1 - \alpha) k_b T_c + \epsilon k_b T_H$$

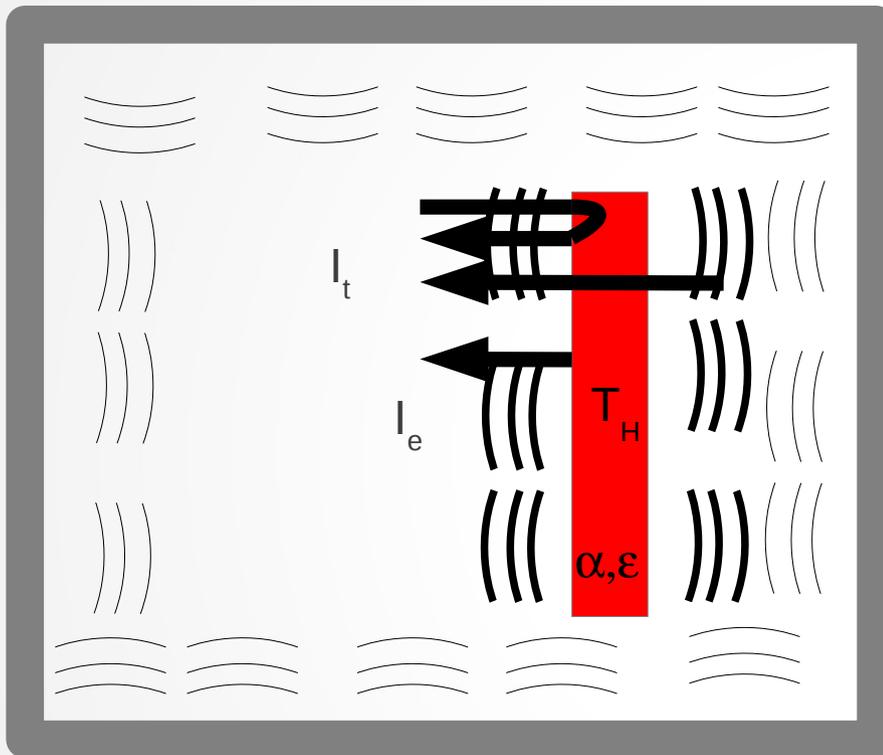
But  $\epsilon = \alpha$  (Kirchoff's law)

$$I \propto (1 - \epsilon) k_b T_c + \epsilon k_b T_H$$

estimation from reflection –  
transmission measurement

$$\alpha = 0.15$$

$$\epsilon = 0.13$$

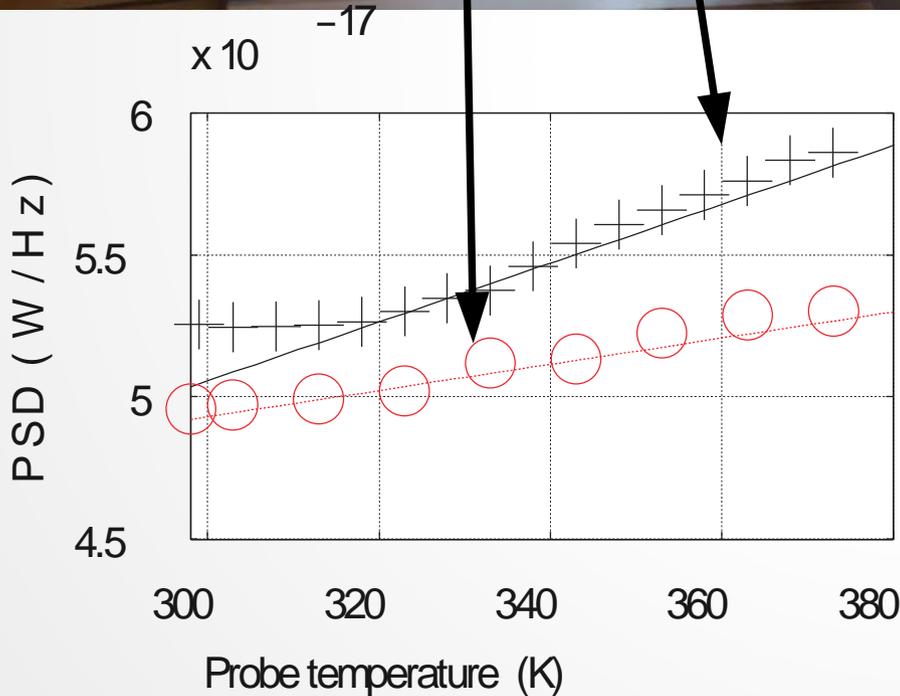


$T_c$

Measured from cross-correlation slope vs. frequency

**Good estimation of the emissivity**

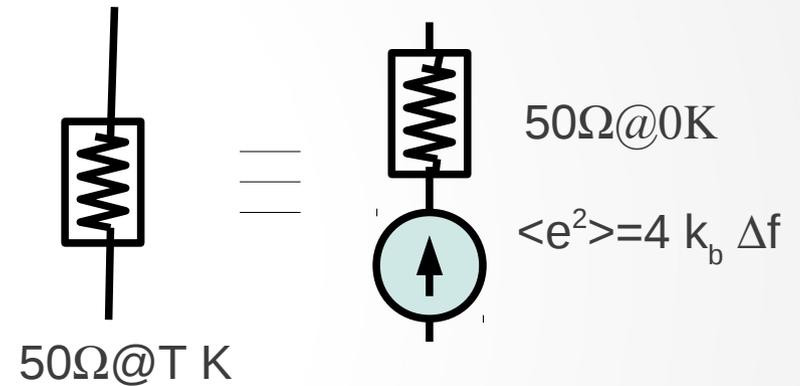
# Power spectrum density in an oven



$T \sim 300 \rightarrow 400^\circ\text{K}$

- Power spectrum density of
- an omnidirectional antenna
  - of a  $50\Omega$  resistance

Resistance model



Johnson–Nyquist noise

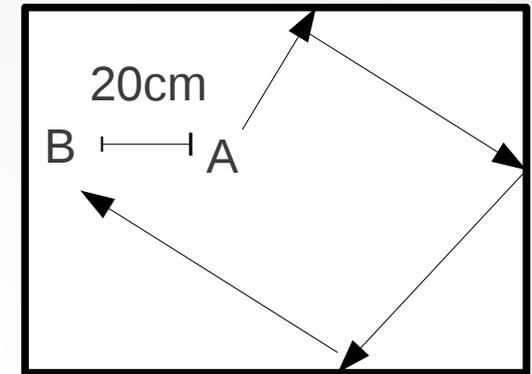
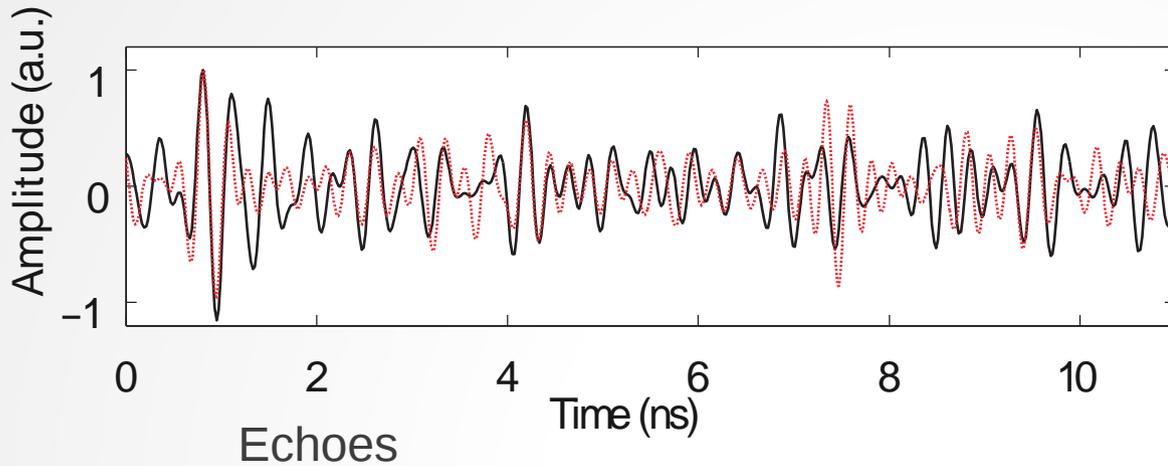
$$\text{PSD of resistor} = k_b T_{\text{OVEN}}$$

$$\text{PSD of cavity} = \epsilon k_b T_{\text{OVEN}}$$

$\epsilon=0.55$  due to cavity losses

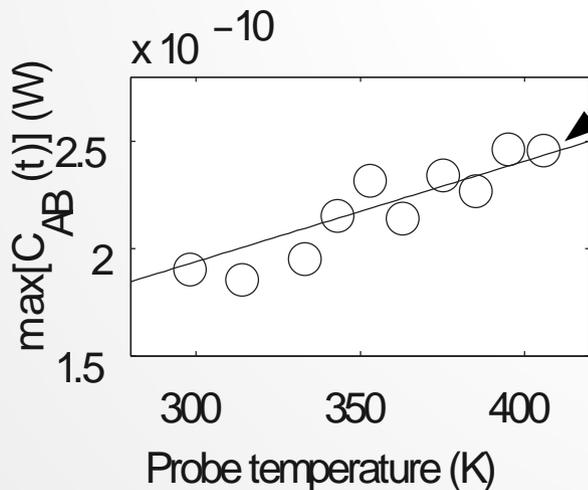
# Cross-correlations in an oven

Cross-correlations between 2 antennas



Oven is a reverberation cavity

Maximum correlation versus temperature

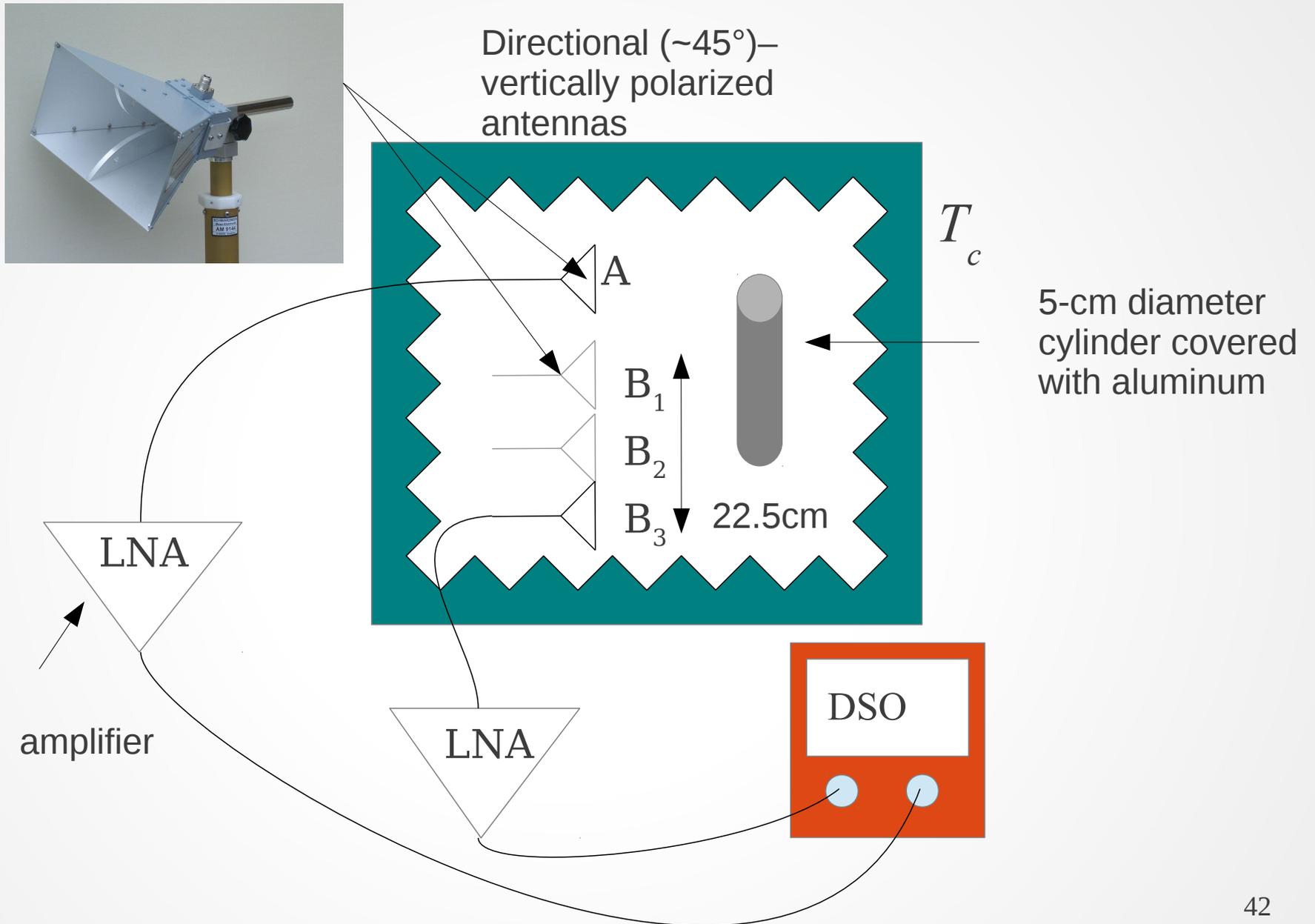


$$C_{AB} \propto (T_0 + \epsilon [T_{OVEN} - T_0])$$

The cavity is leaky (some energy is radiated outside it)  $\rightarrow \epsilon < 1$

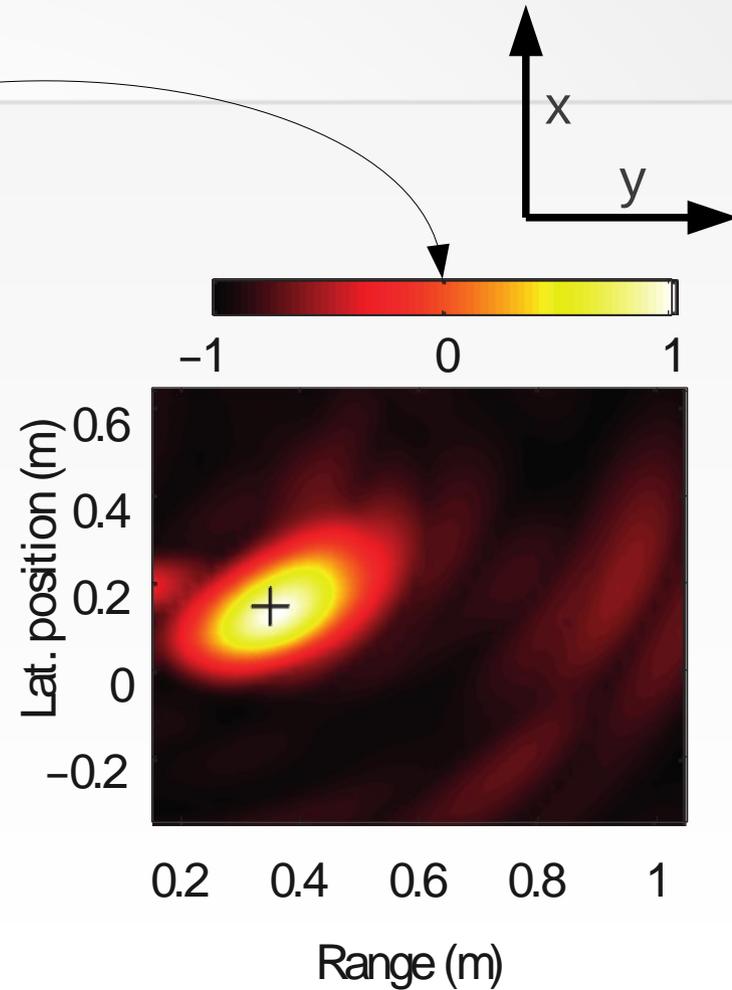
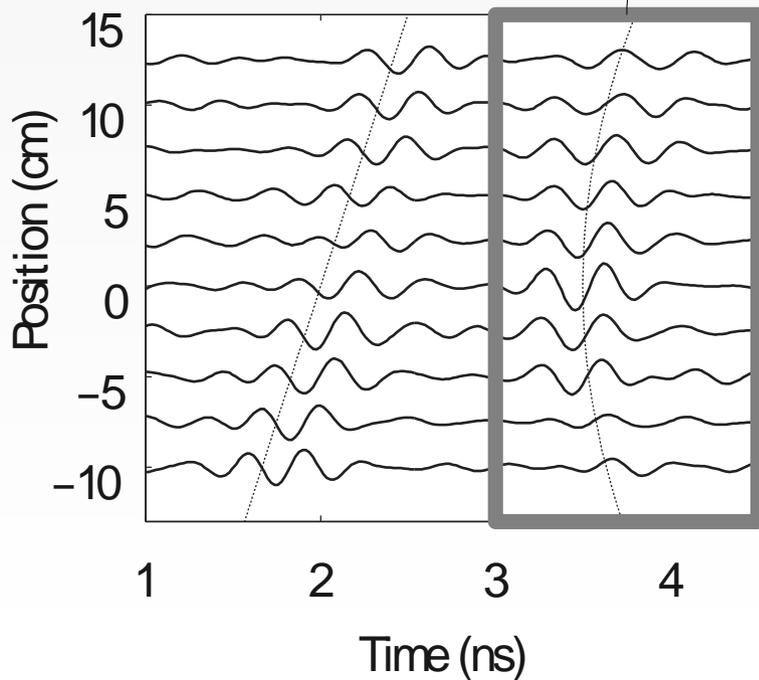
**↓**  
 $\epsilon = 0.6$

# Application to imaging



# Imaging from thermal noise

Causal part of the Green's function



$$I(x, y) = \left| \sum_{\text{positions}} C_{ref, j} \left( t - \sqrt{(y - j \delta x)^2 + x^2/c} \right) \right|$$

Antenna B steps

# Conclusions

- Green's function recovering with electromagnetic waves from
  - Artificial noise
  - Thermal noise
- Fluctuation dissipation theorem
- Black body thermal emission
- Non-uniform temperature → asymmetric pulse reconstruction
- Green's function in hot reverberating media
- Main application : detection / imaging